OGDEN AIR LOGISTICS CENTER HILL AFB UTAH PROPELLANT L--ETC F/G 21/9.2
PROPELLANT SURVEILLANCE REPORT LGM-30 F AND G STAGE 1 PHASE E, --ETC(U)
APR 79 J A THOMPSON
MANCP-416(79)
NL AD-A069 080 UNCLASSIFIED 1 of 2 AD A069 080 Will.

HEADQUARTERS OGDEN AIR LOGISTICS CENTER UNITED STATES AIR FORCE AD A 0 6 9 0 8 0 HILL AIR FORCE BASE, UTAH 84056 PROPELLANT SURVEILLANCE REPORT LGM-30 EAG STAGE 1 PHASE E, SERIES VIL TP-H1011, PROPELLANT LABORATORY SECTION John A. Thompson DOC FILE COPY MANCP-REPORT 416(79)

APPROVED FOR PUBLIC RELEASE, DISTRIBUTION UNLIMITED

107 387 79 05 23 038 PROPELLANT SURVEILLANCE REPORT LGM-30 F & G STAGE 1 (TP-H1011)



Author

Component & Combustion Test Unit

Engineering & Statistical Review By

John K Scambia

SCAMBIA, Project Engineer Service Engineering

Edward J. Exickson, Statistician Data Analysis Unit

Recommended Approval By

Leonidas Brown by LEONIDAS A. BROWN, Chief Component & Combustion Test Unit

Ronald F. Larsen, Chief Physical & Mechanical Test Unit

Approved By

7 Woods DON F. WOODS, Chief Propellant Laboratory Section

April 1979

This document has been approved for public release and sale; its distribution is unlimited.

Industrial Products & Ldg Gear Division Directorate of Maintenance Ogden Air Logistics Center United States Air Force Hill Air Force Base, Utah 84056

05 23 038

ABSTRACT

This report contains propellant test results from cartons of TP-H1011 bulk propellant representing LGM-30 F and G First Stage Minuteman Motors. This report uses a statistical approach to analyze the bulk carton propellant data. Testing was accomplished in accordance with MMWRM Project M82934C-WNL17514.

The data from this test period are combined with data from previous testing and entered into the GO85 computer for storage, analysis and regression analysis. From the statistical analysis of all data tested to date (thirteen years for F and G), significant degradation of the propellant does not appear likely for at least two years past the oldest data point.

Each point on the regression plot represents the mean of all samples at that particular age. The number of samples at each point is indicated on the sample size summary sheet on the page accompanying each regression plot or group of regression plots. The data range at any age can be found by suitable inquiry of the GO85 system.

NTIS DDC UNANNOUNCED JUSCI ICATION	White Section Buff Section
3 v	
DISTRIBUTION/AV	APLABILITY CODES
	SPECIAL

TABLE OF CONTENTS

Abstract to annument adjuster sper pasifagore enlargor from atter	0.000000
List of Figures	7
List of References in any independent of the property of the p	K
	111
Introduction 1	
Table 1 - Test Program	
Statistical Approach 4	
Test Results	
Conclusions 10	
Distribution List	
DD 1473	

on the sample size ammanty sheet on the rays accompanying each regression

LIST OF FIGURES

Figure Nr		Page
	Regression Plot, Very Low Rate Tensile	
1	Strain at Maximum Stress	12
2	Maximum Stress	13
3	Strain at Rupture	14
4	Stress at Rupture	16
5	Modulus	17
	Regression Plot, Low Rate Biaxial Tensile	
6	Strain at Maximum Stress	19
7	Maximum Stress	20
8	Strain at Rupture	21
9	Stress at Rupture	22
10	Modulus	23
	Regression Plot, Low Rate Tensile	
11	Strain at Maximum Stress	25
12	Maximum Stress	26
13	Strain at Rupture	27
14	Stress at Rupture	28
15	Modulus	29
	Regression Plot, High Rate Triaxial Tensile	
16	Strain at Maximum Stress	31
17	Maximum Stress	32
18	Strain at Rupture	33

Figure Nr		Page
19	Stress at Rupture	34
20	Modulus	35
	Regression Plot, High Rate Hydrostatic Tensile	
21	Strain at Maximum Stress	37
22	Maximum Stress	38
23	Strain at Rupture	39
24	Stress at Rupture	40
25	Modulus	41
	Regression Plot, Stress Relaxation .5% Strain, -65°F	
26	Modulus at 10 sec	43
27	Modulus at 50 sec	44
28	Modulus at 100 sec	45
29	Modulus at 1000 sec	46
	Regression Plot, Stress Relaxation .5% Strain, -40°F	
30	Modulus at 10 sec	48
31	Modulus at 50 sec	49
32	Modulus at 100 sec	50
33	Modulus at 1000 sec	51
	Regression Plot, Stress Relaxation 3% Strain, 20°F	
34	Modulus at 10 sec	53
	Modulus at 50 sec	54

Figure Nr		Page
36	Modulus at 100 sec	55
37	Modulus at 1000 sec	56
	Regression Plot, Stress Relaxation 3% Strain, 77°F	
38	Modulus at 10 sec	58
39	Modulus at 50 sec	59
40	Modulus at 100 sec	60
41	Modulus at 1000 sec	61
	Regression Plot, Stress Relaxation 3% Strain, 100°F	
42	Modulus at 10 sec	63
43	Modulus at 50 sec	64
44	Modulus at 100 sec	65
45	Modulus at 1000 sec	66
	Regression Plot, Stress Relaxation 3% Strain, 140°F	
46	Modulus at 10 sec	68
47	Modulus at 50 sec	69
48	Modulus at 100 sec	70
49	Modulus at 1000 sec	71
	Regression Plot, Stress Relaxation 3% Strain, 180°F	
50	Modulus at 10 sec	73
51	Modulus at 50 sec	74
52	Modulus at 100 sec	75
53	Modulus at 1000 sec	76

Figure Nr		Page
	Regression Plot, Sol Gel	
54	Percent Extractables	78
55	Gel Swell Ratio	79
56	Sol Gel Density	81 <i>3</i>
57	Cross Link Density	82
58	Regression Plot, Constant Strain	84
59	Regression Plot, Hardness	86
	Regression Plot, Pressure Time	
60	Maximum Pressure	88
61	Time to Maximum Pressure	89
	Regression Plot, TCLE	
62	Thermal Coefficient of Linear Expansion Below tg	91
63	Thermal Coefficient of Linear Expansion Above tg	92
	Regression Plot, TGA, 9°C rise/min	
64	Ignition Temperature	94
65	Percent Weight Loss at Ignition	96
66	Percent Weight Loss at 250°C Hold	98
	Regression Plot, DTA, 12°C rise/min	
67	, Endotherm	100
68	Exotherm 1	101
69	Exotherm 2	103
70	Exotherm 3	105

Figure	Nr and American	eratr	Page
71		ition Temperature	106
72	Regress	ion Plot, Burning Rate	108
	to set of		

LIST OF REFERENCES

Report Nr	<u>Title</u>	Report Date
	LGM-30 First Stage, Wing I Test Reports	
29A	Test Report (Missile in silo)	13 Jan 64
29B	Zero Time Test Results	29 Jan 64
29C	Zero Time Test Results (Supplement 1)	30 Mar 64
29D	Zero Time Test Results (Aft Closure)	9 Jun 64
29E	Zero Time (Aft Closure Supplement 1)	24 Jun 64
29F	ATP Phase I Test Results	30 Mar 65
29G	ATP Phase I Test Results	19 Aug 65
29Н	ATP Phase I Test Results	10 Sep 65
32A	Zero Time, Wings II-V Test Results	17 Mar 65
32B	Zero Time, Wings II-V Test Results (Aft Closure)	18 Mar 65
32C	ATP Phase I, Wings II-V Test Results	3 Nov 65
49	ATP Phase I, Wings II-V (First Group)	18 Mar 66
53	ATP Phase I, Wings II-V (Second Group)	22 Apr 66
55	ATP Phase I, Wings II-V (Third Group)	29 Apr 66
58	ATP Phase I, Wings II-V (Fourth Group)	6 May 66
61	ATP Phase I, Wings II-V (Fifth Group)	10 Jun 66
66	ATP Phase I, Wings II-V (Sixth Group)	22 Jul 66
76	ATP Phase II, Wing I Test Results	24 Jan 67
78	Zero Time, Wing VI Test Results	3 Feb 67
104	ATP Phase I, Wing VI (First Group)	12 Oct 67
118	ATP Phase II. Wings II-V (First Group)	5 Mar 68

Report Nr	<u>Title</u>	Report Date
126	ATP Phase II, Wings II-V (Second Group	11 Apr 68
130	ATP Phase II, Wings II-V (Third Group)	3 May 68
162	ATP Phase I, Wing VI (Second Group)	30 Sep 69
176	ATP Phase II, Wing VI (First Group)	15 Apr 70
181	ATP Phase III, Wing I	7 May 70
185	ATP Phase I, Wing VI (Third Group)	22 Jun 70
195	ATP Phase III, Wings II-V (Retest)	29 Oct 70
223	Surveillance Report LGM-30 Stage I(TP-H1011)	Sep 71
239	Surveillance Report LGM-30 Stage I (TP-H1011 and TP-H1043)	Apr 72
258	Surveillance Report LGM-30 A & B Stage I (TP-H1011)	Nov 72
268	Surveillance Report LGM-30 A & B Stage I (TP-H1011	May 73
271	Surveillance Report LGM-30 F & G Stage I Phase A Series II, (TP-H1011)	Jul 73
277	Surveillance Report LGM-30 F & G Stage I Phase A Series III, (TP-H1011)	Oct 73
280	Surveillance Report LGM-30 A & B Stage I (TP-H1011)	Nov 73
288	Propellant Surveillance Report LGM-30 A & B, Stage I, TP-H1043	Mar 74
290	Propellant Surveillance Report LGM-30 F & G, Stage I, Phase B, Series I TP-H1011	Mar 74
300	Minuteman Stage I Motor Reliability Improvement Program Surveillance	May 74

Report Nr	<u>Title</u>	Report Date
302	Propellant Surveillance Report LGM-30	Nov 74
313	Stage 1 Propellant Surveillance Report, Propellant Containing Glacial Acrylic Acid	Oct 74
315	Propellent Surveillance Report LGM-30 F & G Stage 1, TP-H1011	Jan 75
316	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Feb 75
319	Propellant Surveillance Report LGM-30 Dissected Motors, Phase VI, TP-H1011	Apr 75
321	Propellant Surveillance Report LGM-30 F & G Stage 1, Phase B, Series II, TP-H1011	Apr 75
325	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Jun 75
328	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Sep 75
330	Propellant Surveillance Report LGM-30 F & G Stage 1, TP-H1011	Oct 75
335	Stage 1 Motor Reliability Improvement Program	Dec 75
337	Propellant Surveillance Report LGM-30 A & B, Stage 1, TP-H1043	Feb 76
339	Stage 1, New MAPO & ERL-510 Qualification	Mar 76
341	Propellant Surveillance Report LGM-30 Dissected Motors, Phase VII, TP-H1011	Mar 76

Report Nr	<u>Title</u>	Report Date
343	Propellant Surveillance Report LGM-30 A & B, Stage 1, TP-H1011	Jun 76
345	Propellant Surveillance Report LGM-30 F & G, Stage 1 Phase B, Series III, TP-H1011	Jun 76
350	Qualification of a New MAPO Source and ERL-510 Curing Agent for Minuteman, Stage 1, UF-2121 Liner	Sep 76
351	Propellant Surveillance Report LGM-30 A & B, Stage 1, TP-H1011	Sep 76
354	Minuteman Stage 1 Motor Reliability Improvement Program Surveillance	Sep 76
358	Propellant Surveillance Report LGM-30 Dissected Motors, Phase VIII, TP-H1011	Oct 76
360	Propellant Surveillance Report LGM-30 F & G, Stage 1 Phase E, Series III, TP-H1011	Nov 76
367	Propellant Surveillance Report LGM-30 A & B, Stage 1, TP-H1011	Apr 77
370	Propellant Surveillance Report LGM-30 F & G, Stage 1, Phase E, Series II, TP-H1011	Apr 77
377	Qualification of a New MAPO Source and ERL-510 Curing Agent for Minuteman Stage 1, UF-2121 Liner	Oct 77
379	Final RIP Report, Minuteman Stage 1 Motor Reliability Improvement Program Surveillance	Oct 77
385	Propellant Surveillance Report LGM-30 A, B, F, & G, Stage 1, TP-H1043	Dec 77
388	Propellant Surveillance Report LGM-30 A & B Stage 1, TP-H1011	Jan 78
390	Propellant Surveillance Report LGM-30 F & G Stage 1, Phase E, Series IV, TP-H1011	Ге Б 78
392	Propellant Surveillance Report LGM-30 Dissected Motors, Phase IX, TP-H1011	Mar 78
393	Propellant Surveillance Report LGM-30 A & B	May 78

Report Nr	OF-Way around Title	Report Date
396	Propellant Surveillance Report LGM-30 F & C Stage I, TP-H1011	G Jun 78
405	Propellant Surveillance Report LGM-30 F & 0 Stage I, TP-H1011	G Oct 78

Propellars Surveyllacon Remort Line 30

4.4

ST ST

GLOSSARY OF TERMS AND ABBREVIATIONS

Aging Trend A change in properties or performance resulting

from aging of material or component

CSA Cross Sectional Area

DB Dogbone

Degradation Gradual deterioration of properties or performance

E Modulus (psi), defined as stress divided by strain

along the initial linear portion of the curve.

EB End Bonded

EGL Effective Gage Length

em Strain at maximum stress

er Strain at rupture

"F" ratio The ratio of the variance accounted for by the

regression function to the random unexplained variance. The regression function having the most significant "F" ratio is used for plotting data. The ratio is also used in detecting signi-

ficant changes in random variation between

succeeding time points

JANNAF Joint Army, Navy, NASA, Air Force Committee

MANCP Propellant Lab Section at Ogden Air Logistics Center

Ogden ALC Ogden Air Logistics Center, Air Force Logistics

Command

r or R The Correlation Coefficient is a measure of the

degree of closeness of the linear relationship

between two variables

Linear The general form of the linear regression equation

Regression is Y = a + bx

Equation

Regression Line representing mean test values with respect to time

S_b Standard error of estimate of the regression

coefficient

GLOSSARY OF TERMS AND ABBREVIATIONS (cont)

Se or Sy.X Standard deviation of the data about the

regression line

Sm Maximum Stress

Sr Stress at rupture

Standard Square root of variance Deviation (S_v)

Strain Rate Crosshead speed divided by the EGL

"t" test

A statistical test used to detect significant differences between a measured parameter and an expected value of the parameter (determines if regression slope differs from zero at the 95%

confidence level)

Variance The sum of squares of deviations of the test results from the mean of the series after division by one less than the total number of test

results

3 Sigma Band The area between the upper and lower 3 sigma limit. It can be expected that 99.73% of the inventory represented by the test samples would

fall within this range assuming that the popu-

lation is normally distributed.

90-90 Band It can be stated with 90% confidence that 90% of

the inventory represented by the test samples would fall within this range assuming that the

population is normally distributed

Significant As used in the statistical sense, means a

difference unlikely to have been the result of random sampling from some specified population.

zd + a = 3 at straight

INTRODUCTION

A. PURPOSE:

Laboratory testing has been performed for thirteen years on First

Stage LGM-30 F and G Minuteman Motor propellant blocks to evaluate

the effects of aging on TP-H1011 propellant. This report contains those

tests conducted on propellant as instructed in MMWRM Test Directive GTD-1C,

Amendment 2, LGM-30 First Stage Operational Propellant Laboratory Testing.

Statistical analysis of the data from tests performed will provide early warning if serious degradation trends develop. Annual evaluation of the propellant provides data for input into engineering reliability analysis for service life predictions.

B. BACKGROUND:

LGM-30 F and G testing was started in 1966 with phase testing at 24 month intervals (Report Numbers 78 - zero time; 104, 162, 185-Phase I: 176, 239, 257-Phase II; 271-Phase III). Report Number 257 was the first time that LGM-30 F and G data were statistically analyzed separately from LGM-30A and B data. The present report is a continuation of testing and statistical analysis.

Zero time testing for LGM-30A, B, F and G was started as soon as possible after receipt of the propellant by MANCP. Data from these tests were used to establish a base line for each test parameter.

The LGM-30F and G propellant test matrix (Table 1) is used to determine the number of specimens to be taken from each propellant loaf and the specific test or tests to which these specimens are to be subjected. Very low rate and low rate tensile specimens are taken on all LGM-30F and G blocks. Specimens for other physical and combustion tests are taken from every third (LGM-30F and G) block.

widtheatter attendance and spent tol again sabtvare Smallegore

its, 139, 257-Phage II; 277-Phase LILL Respect thusber 257 was the first

es como as herrage day 3 des 7 3 dell'atte rel retrese mate man

wasts more said. Show to small profe and to release raths wideless

TABLE 1

SAMPLE PLAN

The Procedure for determining tests to be performed on propellant batch samples of LGM-30 F & G First Stage Motors are as follows:

- 1. Divide the USAF motor serial numbers into three groups by dividing the last three digits of each serial number by three to determine the remainder integer, e.g., $154 \div 3 = 51$ with a remainder integer of 1.
- 2. Use the remainder integer to enter the following matrix to determine the group of tests to be performed on the forward, middle, and aft batch samples associated with a particular motor serial number.

TP-H1011 PROPELLANT BATCH SAMPLE	GROUP I	GROUP II	GROUP III
Forward		2	0
Middle	0		2
Aft	2	0	

Each group will receive the following tests:

		8					
	GROUP III	High Rate Hydrostatic	Sol Gel	DSC	TGA	DTA	Impact
TEST MATRIX	GROUP II	Dynamic Response	Stress Relaxation	Burning Rate	Heat of Explosion	Pressure Time	10 10 10 11
	GROUP I	High Rate Triaxial	Creep	Biaxial Low Rate	TCLE	Hardness	Ignitability

NOTE: Low Rate and Very Low Rate Tensile tests are performed on all blocks.

STATISTICAL APPROACH

In order to determine aging trends for shelf/service life predictions, as directed by Service Engineering, First Stage LGM-30 F and G Minuteman TP-H1011 propellant blocks have been undergoing testing since 1966, statistically analyzed and reported on a regular test cycle by this laboratory.

The primary reason for performing statistical analysis on test data is for the detection of propellant changes due to aging that would affect motor reliability. Regression analysis was the method used to examine data and to aid in drawing conclusions about dependency relationships that may exist i.e., relationship between age versus test results.

In selecting the best fit model for the regression equation, the linear model Y = a + bX was found to be the best fit model for 96% of the regression plots. The model used is shown in the regression equation at the top of every regression plot and those which are not linear will also be listed and discussed in the test results section.

Individual data points from different time periods were used to establish a least squares trend line for the data. The variance about the regression line, obtained using individual values of the dependent variable, was used to compute a tolerance interval such that at the 90% confidence level 90% of the sample distribution falls within this interval. This tolerance interval was extrapolated to a maximum of 24 months into the future from age of the oldest motor tested. The 't' value and the

significance of this statistic, which are reported for each regression model, give an indication of the "statistical significance" of the slope of the trend line as compared to a line of zero slope. Data were plotted by computer. The 'y' axis is computed so that the values at one inch intervals are peculiar to the data spread of the parameter tested. Plotted data points represent means at the particular ages at which testing occurred. The number of specimens at each age point is indicated on the sample size summary sheet accompanying the regression plot. Variance at each test age can be determined by consulting the GO85 data storage system.

A post cure effect (propellant stabilizing after the first year or two) has been observed on some of the early test data (stress relaxation at -65°F, -40°F, and 20°F; TGA percent weight loss at 250°C; DTA exotherm 1, and exotherm 2); which tended to bias and skew the projected trend lines.

To overcome this factor, two methods of analysis were performed: First, where possible, non-linear models were used that would best fit the total data (TGA)

Weight loss at 250°C, DTA exotherm 1 and exotherm 2 data); second, where non-linear models did not fit the data as good as the linear model this early data was eliminated (Stress Relaxation at -60°F, -40°F, and 20°F data).

By compensating for this post cure biasing a more accurate aging trend line for service life prediction is provided.

TEST RESULTS

VERY LOW RATE TENSILE:

Very low rate regressions show no significant change for strain at maximum stress with strain at rupture showing a statistically significant decrease. The stresses and modulus show a statistically significant increase (Figures 1 thru 5). The trends are gradual for the respective regressions and no operational problems from the propellant are expected for at least two years beyond the last test date.

LOW RATE BIAXIAL TENSILE:

The strain regressions show a statistically significant gradual decrease.

The stresses and modulus show a statistically significant increase (Figures 6 thru 10).

LOW RATE TENSILE:

Low rate tensile data regressions show a statistically significant gradual decrease for strains and a statistically significant increase for stresses and modulus (Figures 11 thru 15).

HIGH RATE TRIAXIAL TENSILE:

The strain at maximum stress, strain at rupture and modulus regressions show a statistically significant decrease. Maximum stress and stress at rupture do not show a significant change (Figures 16 thru 20).

HIGH RATE HYDROSTATIC TENSILE:

The strains show a statistically significant decrease and the stresses show a statistically significant increase. The modulus did not show a significant change (Figures 21 thru 25).

TENSILE SUMMARY:

The test data regressions show that the strain is gradually decreasing and the stress and modulus gradually increasing.

Based on the analysis of test data regressions, it does not appear that meaningful degradation is occurring at this time and no operational problems are expected in the propellant for at least two years beyond the last data point.

STRESS RELAXATION MODULUS:

For the 0.5% strain at -65°F, the regressions for data at 10, 50 and 100 seconds show a statistically significant gradual increase with the 1000 second regression showing no significant change (Figures 26 thru 29).

At -40°F, the 10, 50, 100 and 1000 second regressions show a statistically significant decrease (Figures 30 thru 33).

The 3% strain regressions at 20°F, 77°F, 100°F, 140°F, and 180°F show a statistically significant gradual increase except for the 20°F at 10 second regression which does not show a change (Figures 34 thru 53).

SOL GEL:

The percent extractables and density do not show a significant change. Gel swell ratio and crosslink density regressions show a statistically significant increase (Figures 54 thru 57).

CONSTANT STRAIN:

A statistically significant gradual decrease is shown for constant strain (Figure 58).

HARDNESS:

Shore A ten second hardness shows a statistically significant increase (Figure 59).

SUMMARY OF SOL GEL, TENSILE AND HARDNESS DATA:

The crosslink density, constant strain and hardness data regressions correlate with the tensile data. As the polymer continues to crosslink, the strains decrease and the stresses and hardness increases.

PRESSURE TIME:

Maximum pressure and time to maximum pressure shows a statistically significant gradual decrease (Figures 60 and 61).

TCLE (Thermal Coefficient of Linear Expansion)

The thermal coefficient of linear expansion for both above and below the glass transition point (Tg) shows a statistically significant gradual increase (Figures 62 and 63).

TGA (Thermal Gravimetric Analysis):

A statistically significant increase is shown for the ignition temperature (9°C rise/min) and the percent weight loss at 250°C hold (12°C rise/min to

hold) with the weight loss at ignition showing no significant change (Figures 64 thru 66). The model Y = a + b ($\frac{1}{x}$) was found to better represent the data than the linear model in Figure 66.

DTA (Differential Thermal Analysis):

The endotherm and first and second exotherms show a statistically significant decrease. The third exotherm and ignition temperature shows a statistically significant increase (Figures 67 thru 71). The model Y = a + b (LOG X) was found to better represent the data on Figures 68 and 69 than the linear model.

BURNING RATE:

The burning rate shows a statistically significant gradual increase
(Figure 72).

THERMAL AND COMBUSTION SUMMARY:

The time to maximum from the pressure time data and burning rate data show a correlation. In both cases, the regressions show a gradual increase in rate of reaction.

The ignition temperatures for TGA and DTA show a gradual increase.

From the analyses of the regressions, no combustion problems are expected for at least two years beyond the oldest data point.

CONCLUSIONS

Thirteen years of aging at ambient temperature (77°F) has not greatly changed the properties of the propellant. Some test parameters indicate slight aging trends, but nothing that would adversely affect the operational characteristics of the rocket motor propellant.

From the statistical analysis, it does not appear that significant propellant degradation is occurring. Based on thirteen years of accumulated data, there is no reason to suspect that properties will show much change for at least two years past the last data point.

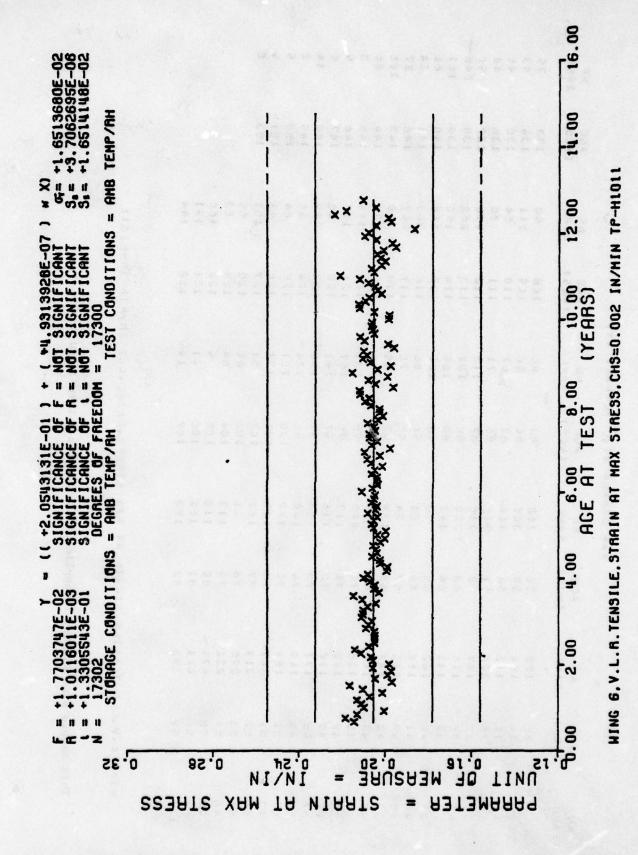
Therefore, propellant reliability should not change appreciably over that time period. Since failure limits are not available for the parameters tested, this statement is based on the fact that the slope of the regression curves where statistically significant are, with few exceptions, relatively flat or close to the line of zero slope and have not changed appreciably from the last test period.

4# SANFLE SIZE SUMMARY

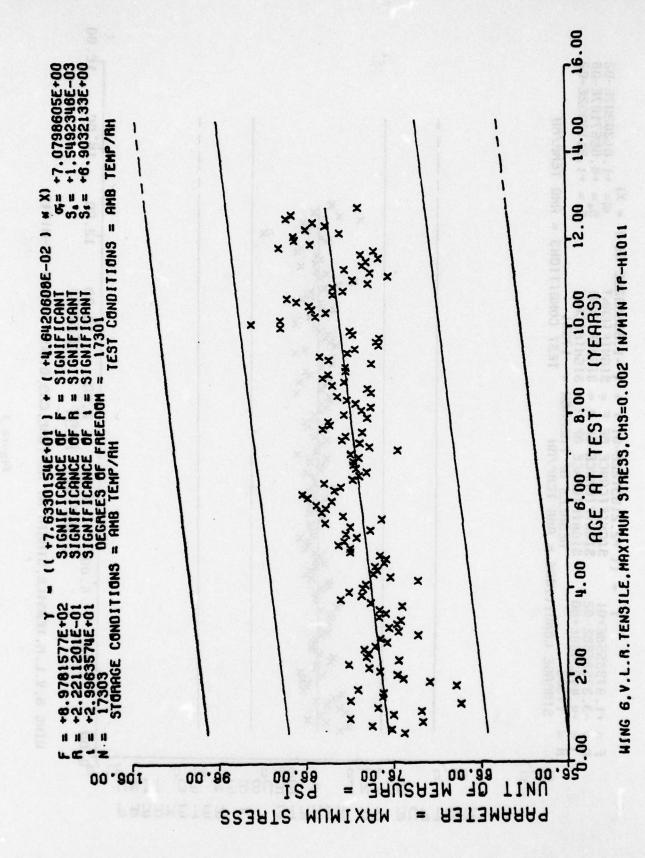
4	SANE	54.	63	4.5	48	0.5	246/	151	99	4:	27	165	EE	r)	5	v	14	ניו	5	5	u)						
AGE	(NCS)	133	134	135	136	137	138-	139-	140	141	142	143-	144	145	146	147	148	149	150	151	153						
A R	SANE	. 05		45	30	116	262	150	116	363-	247	140	133	351	117	16	42	36	84	44	101	60	63	166	151	144	
AGE	(NCS)	108	531	110	1111	112	113	114	116	116	117	118	119	120	151	122	123	124	125	126	127	128	129	130	131	132	
32	SANF	96	6 €	67	7.1	113	127	.591	125	96	2.0	56	06	131	167	141	150	1747	151	121	5.1	9	40	UT.	11	16	
A GE	(408)	83	84	65	B	87	96	en O	05	15	25	53	95	35	96	25	98	66	100	101	1 62	103	104	105	106	107	
R A	SANF	3.52	306	466/	266	316-	228	142	0.5	6.1	24	134	156	245	117	116	63	140	177	135	161	15	117	110	152	153	
AGE	(NOS)	w u	(F)	60	19	62	ė3	64	6.51	66	67	99	89	7.0	7.1	7.2	73	74	75	7.6	77	78	52	90	1 E	62	
34	SANE	162	154	113	22¢	147	126		122				1 Cé	177			177	159	168	4	314	U	232	~			
AGE	(804)	33					a e			41																	
N.	AND	r,	1.9		1.5		33 4			40								47				90	40		88	153	
uı	9	w	C.	91	11	12	13	14	1.5	16	17					N	S		CA		27				31		

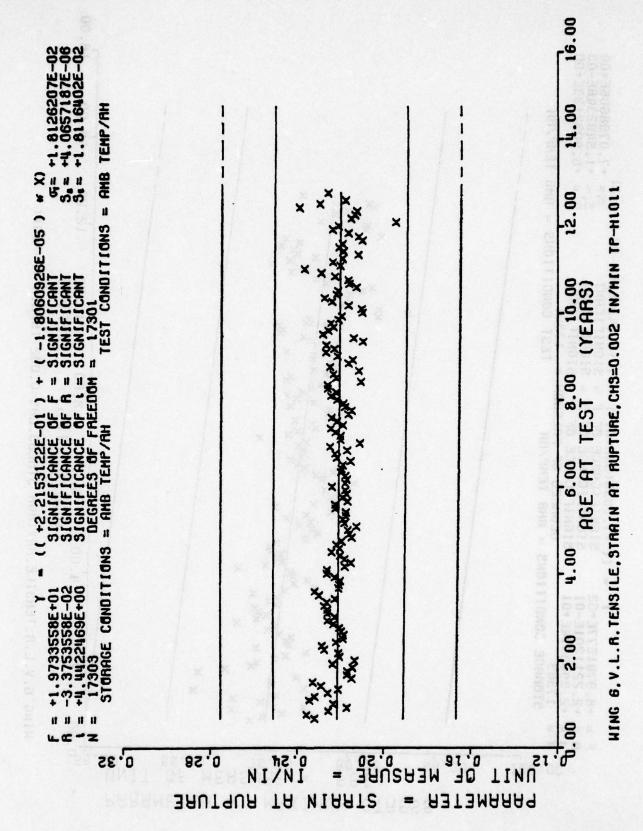
WING COVOLOFOTENSILE, STRAIN AT MAX STRESSOCKS=0.002 IN/WIN TP-HIOII

This sample size summary is applicable to figures 1 thru 3 and 5.



- 12 -



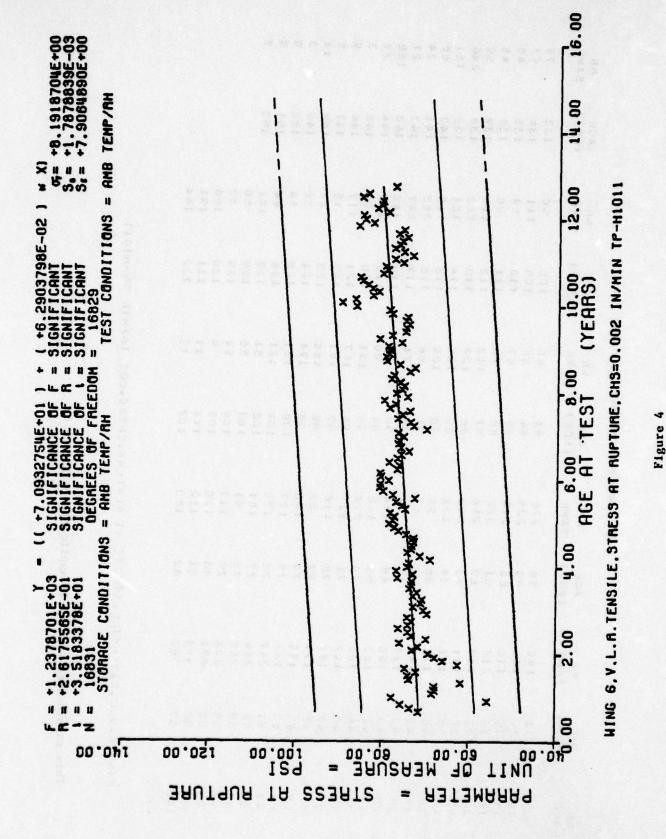


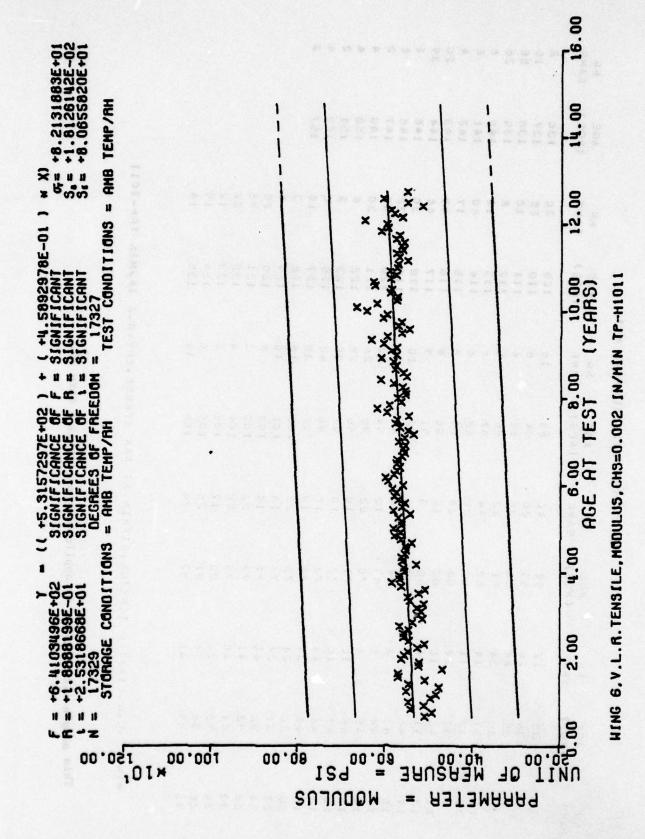
*** SAMFLE SIZE SLMWARY ***

N A S	54	53	45	46	05	246	151	99	4:	27	185	EE	m	5	•	=	۳)	5	5	4)					
(NCS)	133	134	136	136	137	138	136	140	141	142	143	144	145	146	147	148	149	150	151	153					
SARF	35	==	€.	30	118	262	151	118	303	247	140	133	156	1117	16	42	36	8.	44	101	6.0	F)	166	151	144
AGE (NCS)	108	109	110	1111	112	113	114	116	116	117	116	119	120	121	122	123	124	125	126	127	128	129	130	131	132
SARF	38	96	6.7	20	113	127	155	125	86	2.0	55	06	131	167	141	150	174	151	121	51	t) (O	54	(J)	11	0
, AGE (NCS)	60	4.0	æS	98	187	£.	68	05	1.5	25	63	75	95	96	26	96	66	100	101	102	103	164	105	1 C6	107
SANE	276	238	315	222	286	205	138	35	ć.1	24	134	198	246	117	116	E.3	140	177	136	161	15	117	110	152	1.0
(NOS)	58	55	60	19	62	63	40	0,0	99	67	68	9.0	20	7.1	72	7.3	74	7.5	76	77	7.8	13	90	91	2.5
S A S I	140	139	116	216	136		110	116	541 .		120	163	13.0	W	166	177	5	-	347	314		P)	-	·	
(NOS)	33	34	35	40	37	36	ON ITS	40	4.1	42	43	44	46	46	47	4	54	50	51	52	C)	54	96	56	57
SANF	m	51		16	36	4 E	23	36	46	u)	28	5+	24	90	27	67	e e	63	47	0.3	56	40	73	9	148
AGE (NCS)	æ	v	01	11	12	27	14	16	16	17	13	51	50	2.1	w	52	N	N	26	27	28	52	36	31	3.2

WING G.V.L.F. TENSILE, STRESS AT RUPTURE, CHS= 6.002 IN/MIN TP-H1011

This sample size summary is applicable to figure 4.



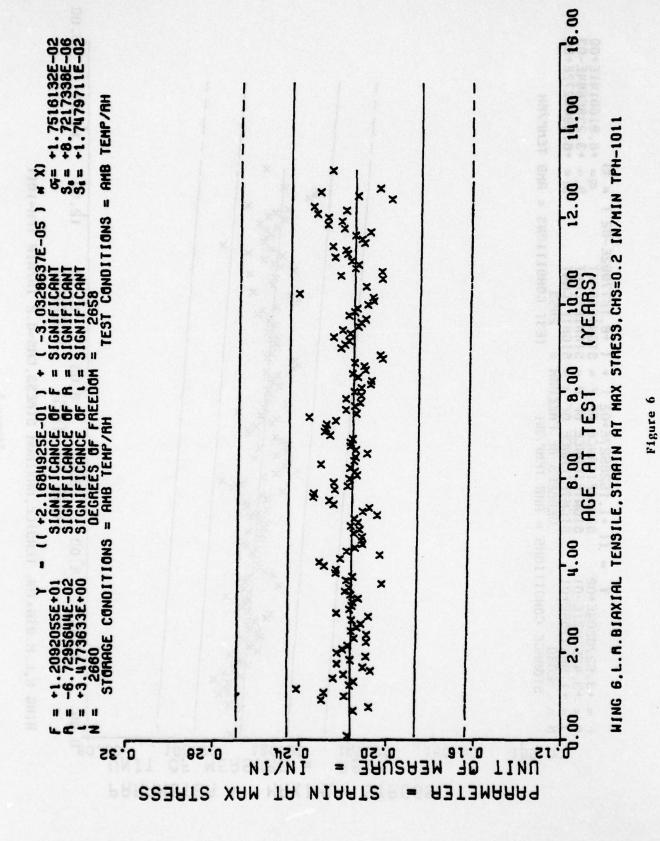


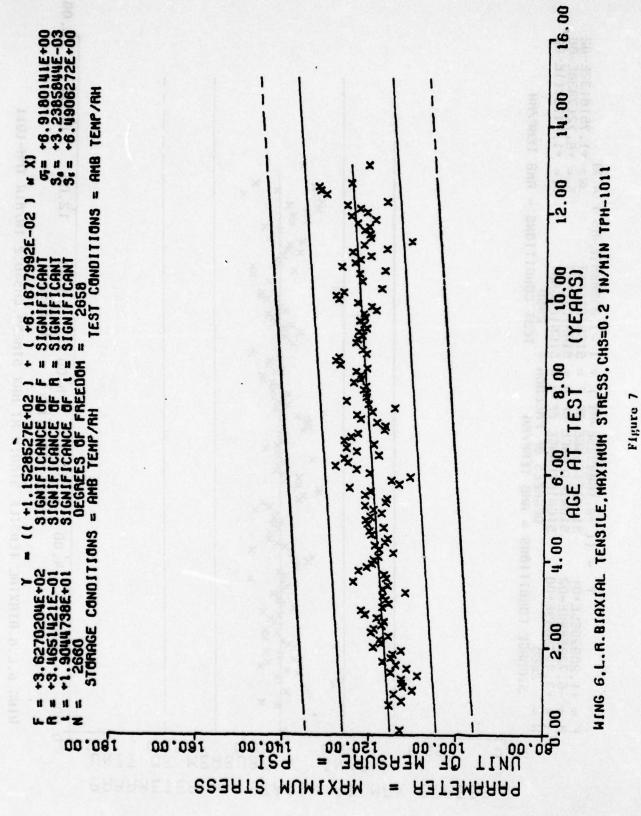
*** SAMFLE SIZE SLMPARY ***

7.	SANE	N	-15	26	36	9	w	₹.	20	38	"	9	~	•	•	8	*	W								
AGE	(MOS)	136	137	138	135	140	141	142	143	144	146	146	147	149	150	151	162	157								
R.	SAND	20	80	10	w			17					42		w	(V	v	01	m	v	50	76	22	12	15	• •
AGE	(100)	109	110	1111	112	113	114	115	116	117	118	119	150	121	122	123	125	127	128	129	130	131	132	133	134	75.1
N.R.	SANF	16	æ	4	w w	v	¥	æ	¥	~			23								w	ניז	4	N	Û	
AGE	(824)	£3	94	65	98	87	8.9	68	05	15	92	63	45	35	95	16	96	66	100	101	102	103	1 C4	105	106	000
NR	SANE	4	26	90	22	44	36	60	10	₅	¥	4	12	22	10	10	16	1.8	(D)	14	51	22	2 C	17	25	* 0
AGE	(SON)												69													
N.F.	SANE			26								W	w	•				34								
AGE	(NOS)	33	34	נט פא	36	37	36	35	4 C	4.1	42	7	44	4	4	47	46	54	חו	מי	יש	מי	6.0	35	56	ריי
N.N.	SAMP		N	4	0	14	22	4	16				14													
AGE	(50%)	-	œ)	5	=	12	13	+-	15	91	17	16	13	20	21	CA	N	8 24	W	26	27	35	25	30	31	Cr

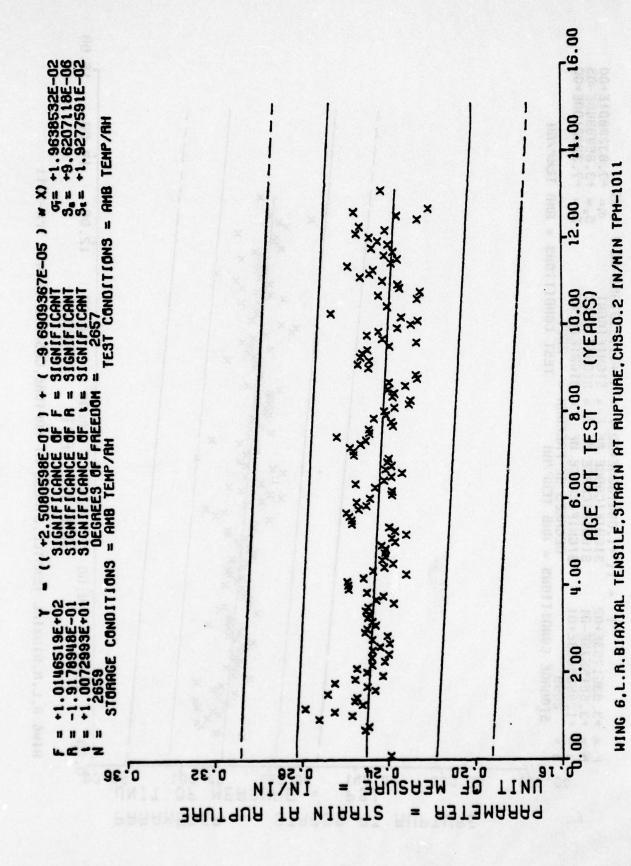
WING C.L.R.EIAXIAL TENSILE, STEAIN AT NAX STRESS, CHS=0.2 IN/MIN TFF-1011

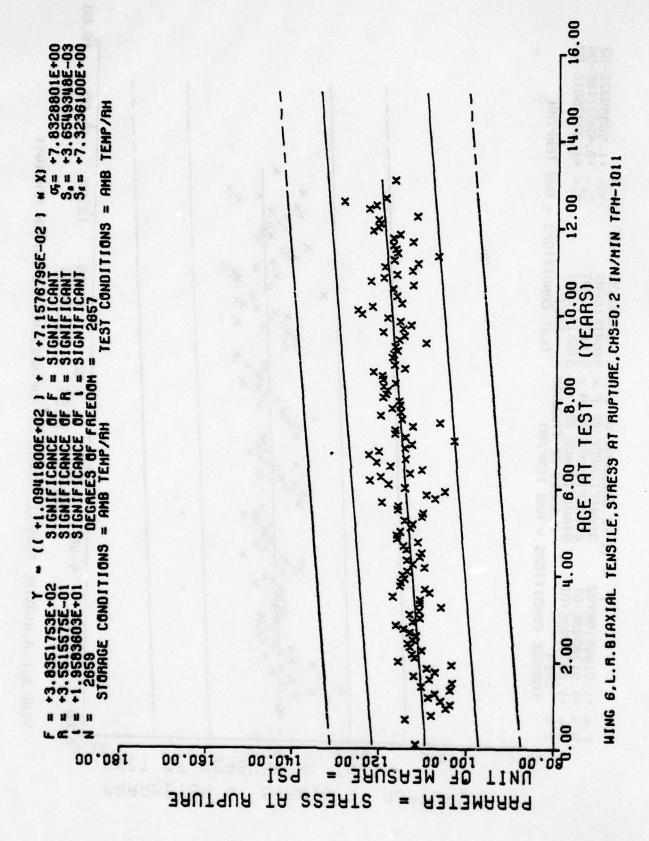
This sample size summary is applicable to figures 6 thru 10.

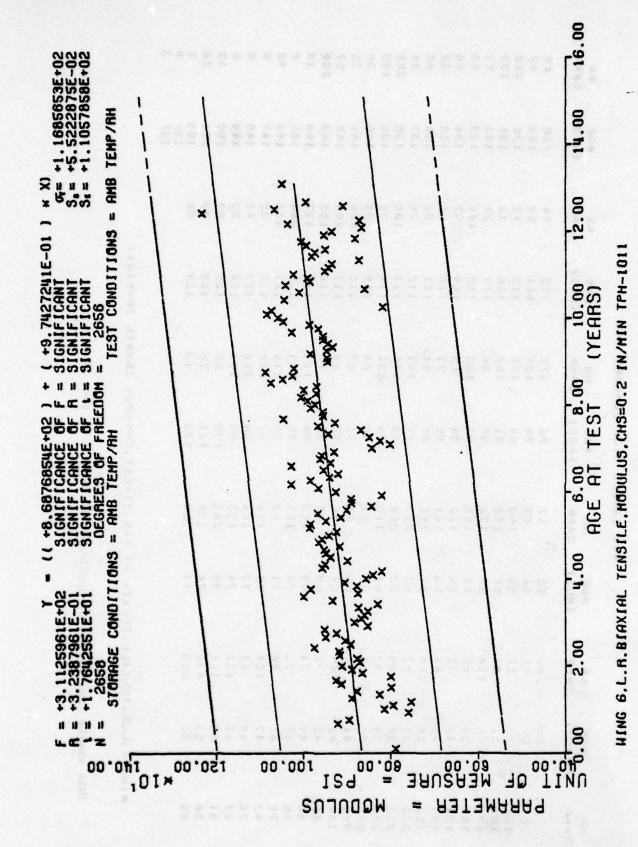




- 20 -





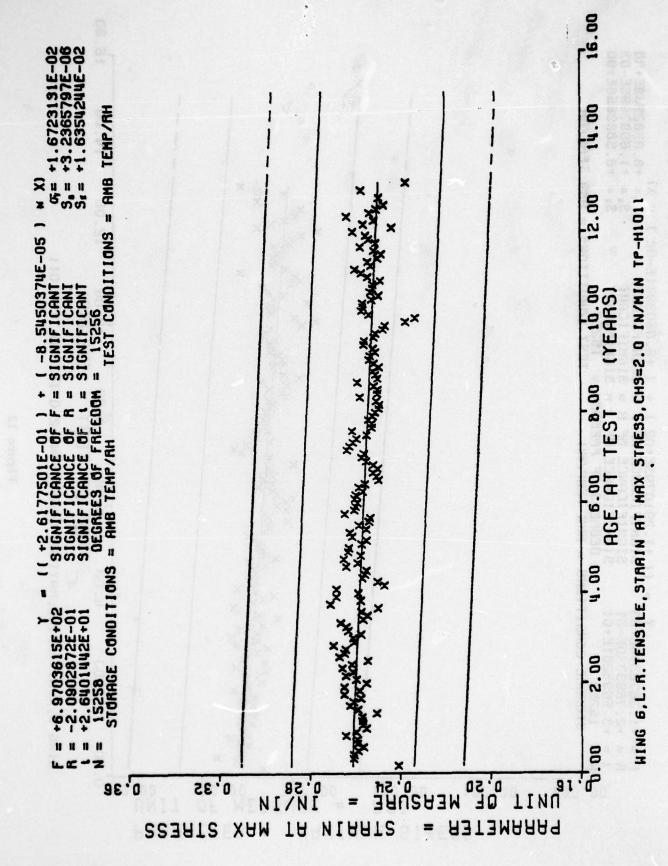


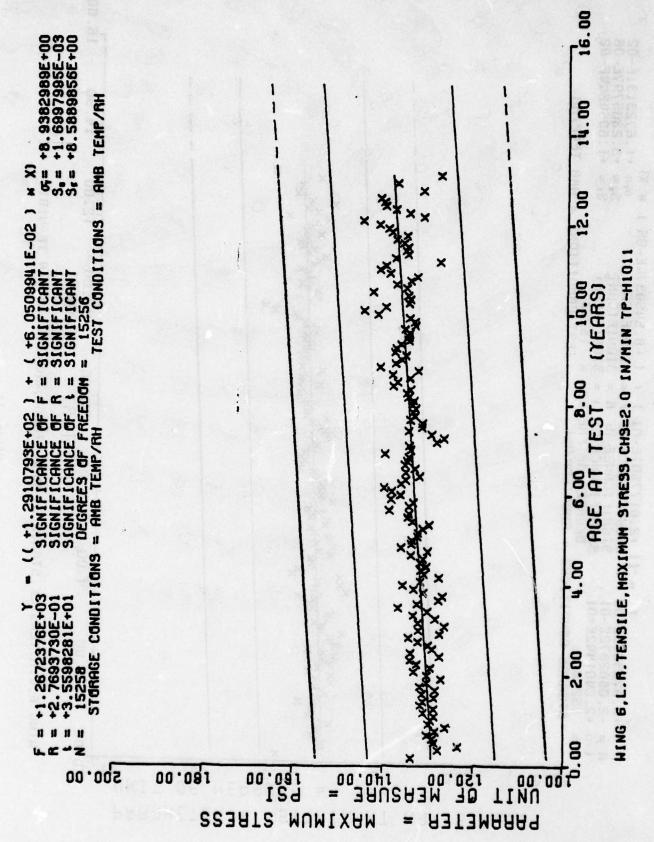
+++ SAMFLE SIZE SUMMARY +++

4 4	66	45	252	132		90	05	35	4.	64	252	163	34	() ()	23	206	18	•	15	5	•	9	12	2	m	9	3
AGE (HOS)	128	129	130	131	132	133	134	135	136	137	138	139	140	==	142	143	144	145	146	147	148	149	150	151	153	155	157
A 4 8	:	57	12	12	27	105	46	99	30	76	301	20	68	264	261	152	117	244	103	W) P)	•	33	57	72	88		
AGE (PCS)	103	104	105	931	101	108	601	110	111	112	113	1114	115	911	117	118	119	120	121	122	123	124	125	126	127		
SAN	171	125	132	162	86	001	59	11	51	141	126	135	84	67	980	72	113	121	512	230	200	141	99	92	13		
16E (10S)	78	19	80	91	82	83	84	85	98	87	88	68	05	16	92	63	*6	35	95	16	98	66	100	101	102		
SAN	2.5	63	143	106	172	156	122	141	166	203	262	110	61	04	3.6	65	103	163	67	131	144	172	241	156	164		
AGE	53	5.4	55	56	57	58	55	60	61	62	63	64	6.5	99	67	68	69	0.2	7.1	72	73	74	75	76	11		
SAR	6	u)	(2)	(4)	124	£5	36	:	154	63		53	6.5	W)	53	75	21	20	56 6	106	£.	122	106	175	223		
AGE	26	29	30		32			36	36		36	36	04		42		:	4.6	46	47	48			51			
S A A B	m	57	151	161	171	143	154	185	152	220	213	222	223	-	184	26	99	91	7.8	43	36	77	21	95	56		
AGE (MCS)	"	•	w	v	1	æ	v.	10	=	12	13	-	10	91	. 17		-				63						

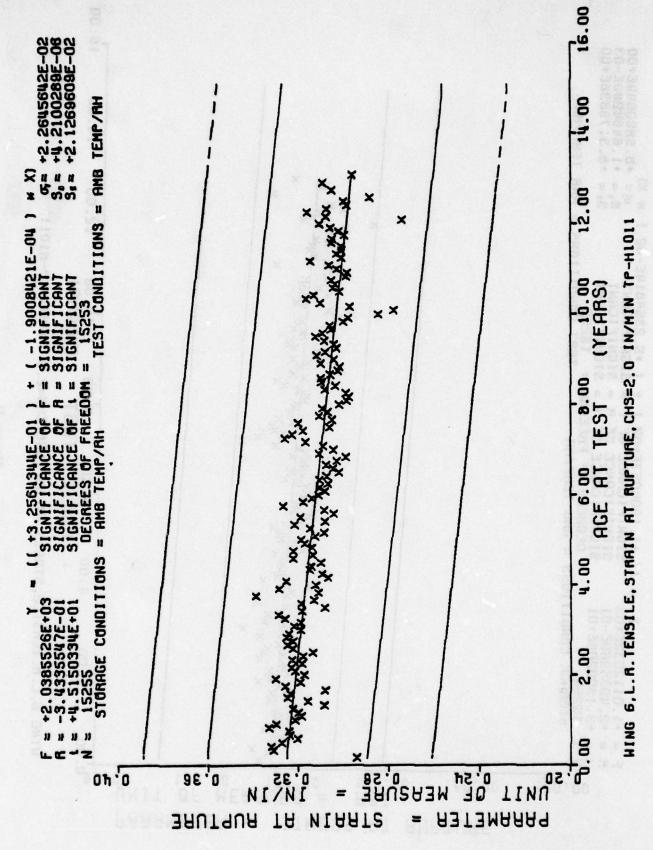
WING C.L.R. TENSILE. STRAIN AT MAX STRESS, CHS=2.0 IN/WIN TF-F1011

This sample size summary is applicable to figures 11 thru 15





- 26 -



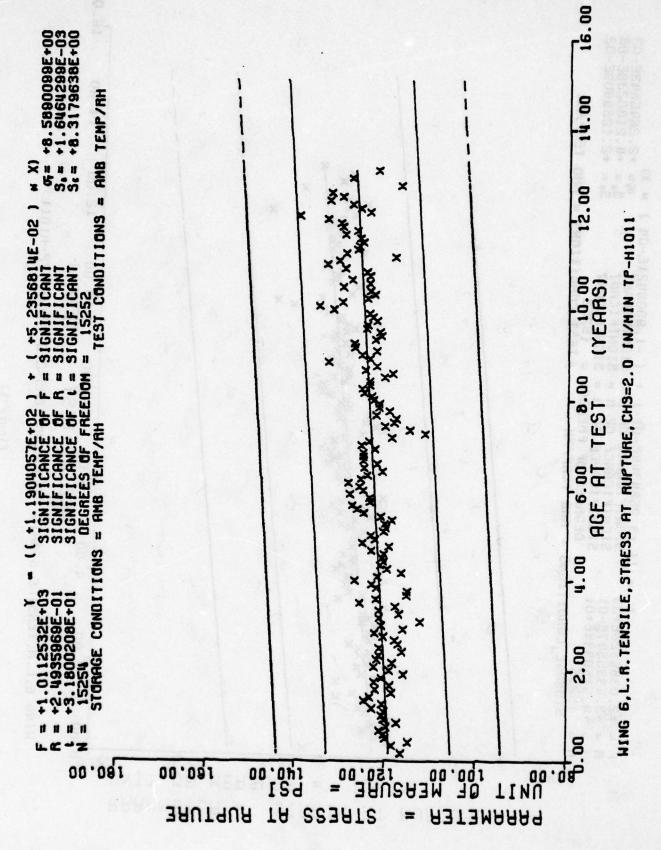
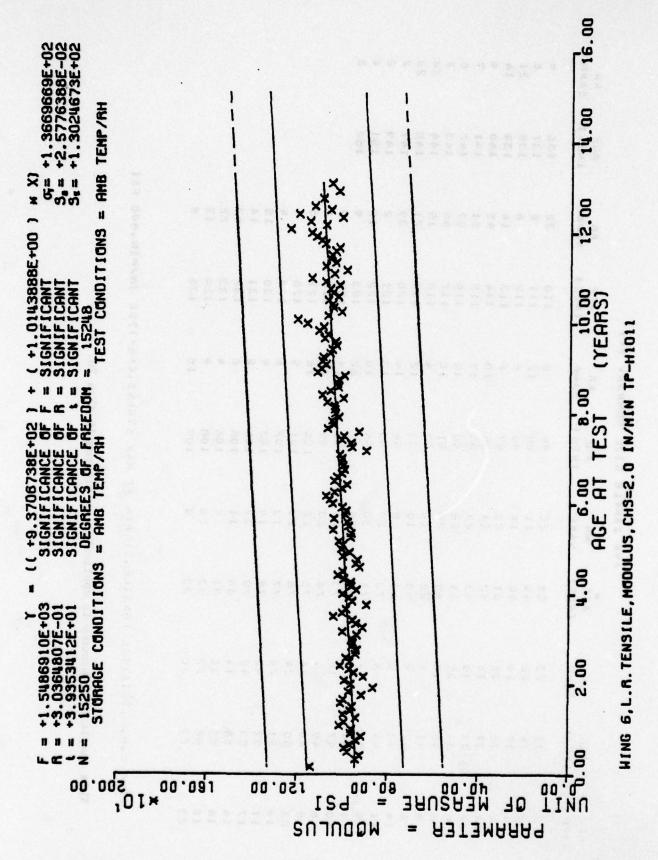


Figure 14

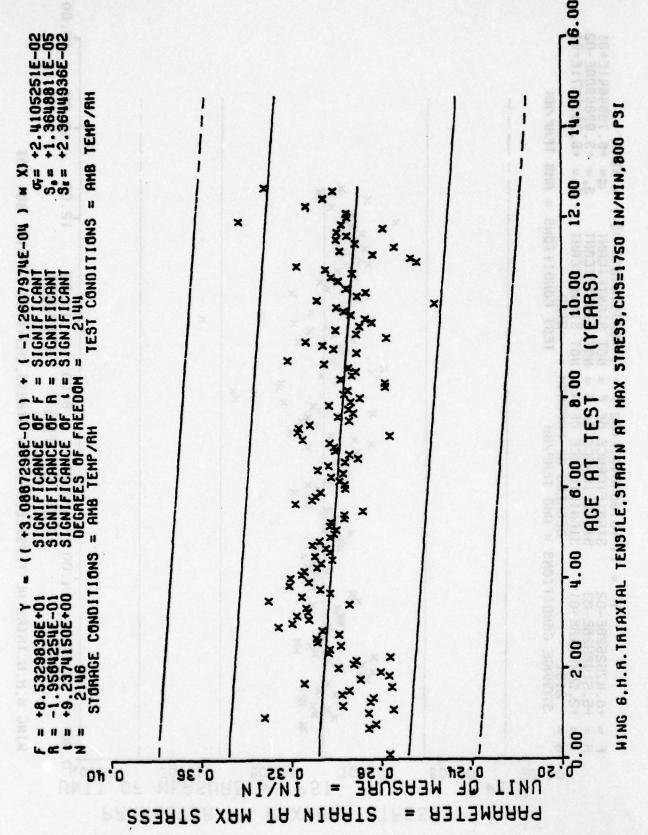


*** SAMFLE SIZE SUMMARY ###

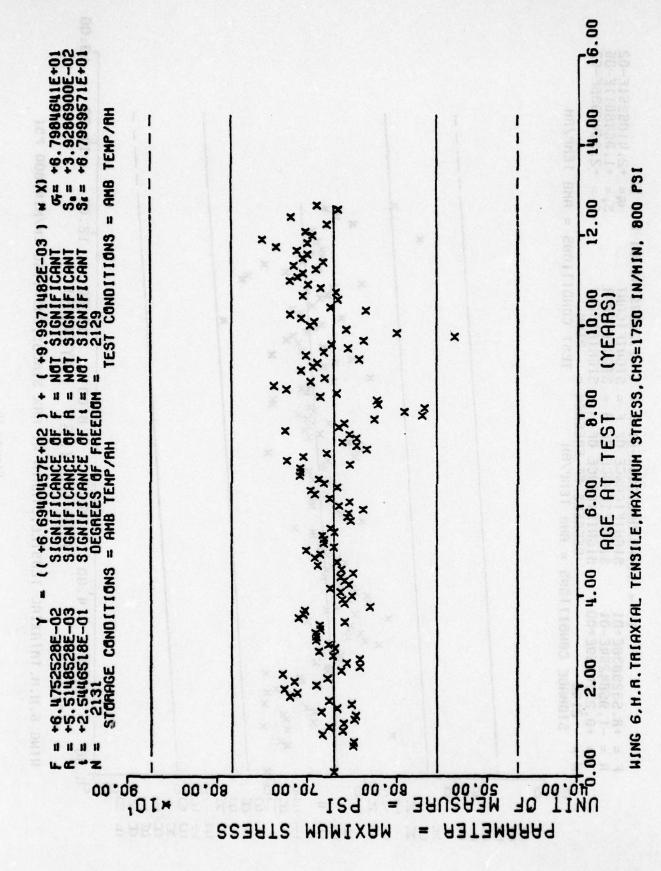
4	SAPP	•	æ	51	=	4	7	•	~	36	23	2	8	•	~												
AGE	(MOS)	136	137	138	139	140	141	142	143	141	145	147	149	151	152												
ž	SANP	32	au	•	4.	4 6	51	57	0.4	19	21	39	N	12	0	2	8	v	•	•	15	<u>:</u>	43	26	12	æ	
ACE	(NCS)	110	111	112	113	114	115	911	117	118	119	120	121	122	123	124	125	127	128	129	130	131	132	133	134	135	
Z.	SAMP	v	12	ý	Œ	10	17	15	1 e	4	12	14	12	91	22	16	56	91	v	O.	•	(V	y	•	œ	16	
A GE	(MCS)	84	85	96	44	98	6.60	05	91	25	93	45	55	95	46	96	66	100	101	102	1 03	104	105	106	108	109	
Υ Z	SANE	0 17	13	1.4	23	24	23	28	20	1.0	01	y	28	30	15	24	23	(3	20	13	14	27	14	Ç	22	y.	
AGE	(80%)	e) to	53	50	10	52	6,3	90	65	99	68	59	20	7.1	72	7.3	74	75	92	77	78	4	90	18	92	93	
ď	SANE			24	26		1.1	(N		ē.	Ç	(V	4	8	¥	16	σ.	34	34	24		42	14		2.2		
AGE	(NCS)	33	34	S. E.	36	37	33	88	40	41	42	43	44	45	46	47	4 8	64	20	51	52	53	54	53	56	57	
X	SAMP	2	2	7	+	•-	1.7	0	۰0	ю	4	14	111	20	4	10	•	•	23	13		17	41	18	91	23	
AGE	(NGS)	-	æ	ď	11	12	13	14	15	16	17	18	1.5	20	2.1	22	23	24	25	26	27	28	53	30	31	63	

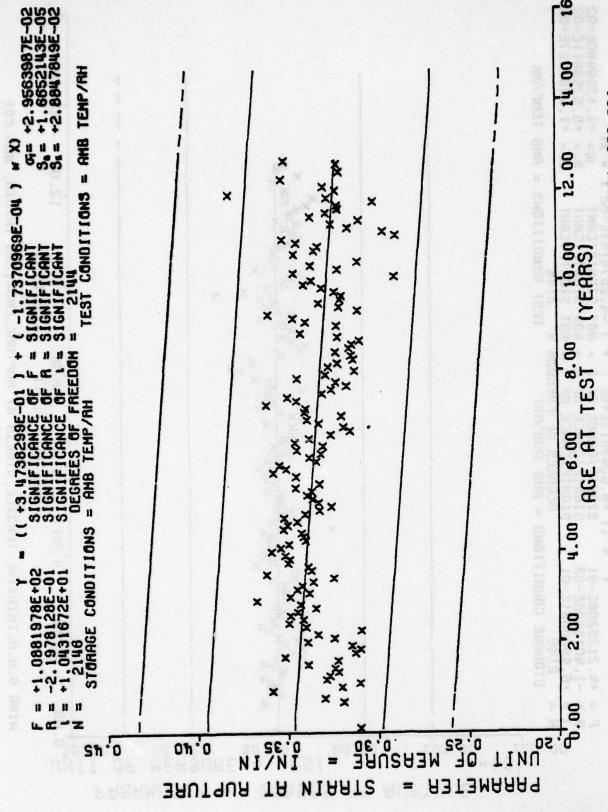
WING E.F.R. TRIAXIAL TENSILE STRAIN AT MAX STRESS, CHS= 1750 IN/MIN, 800 FSI

This sample size summary is applicable to figures 16 thru 20.

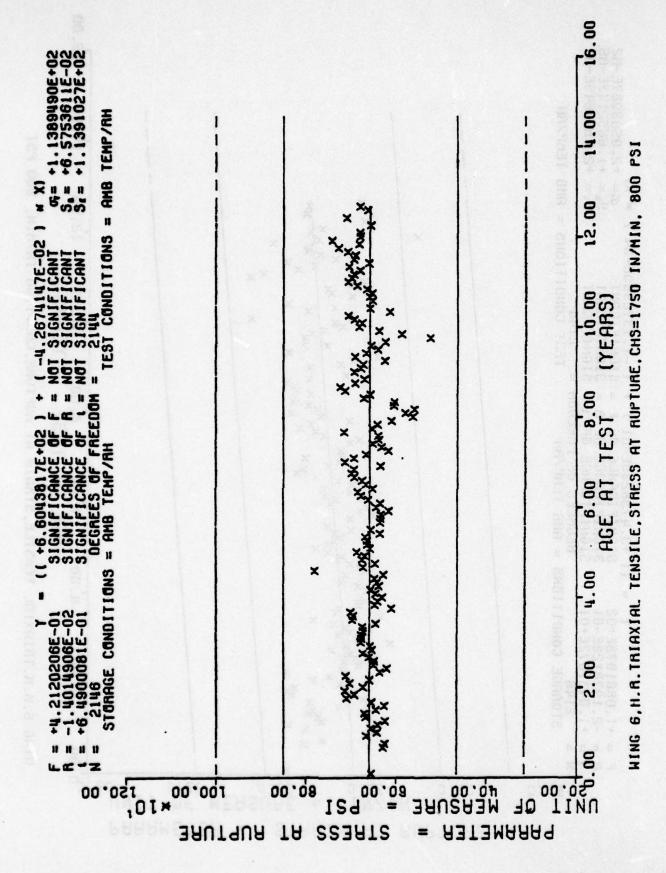


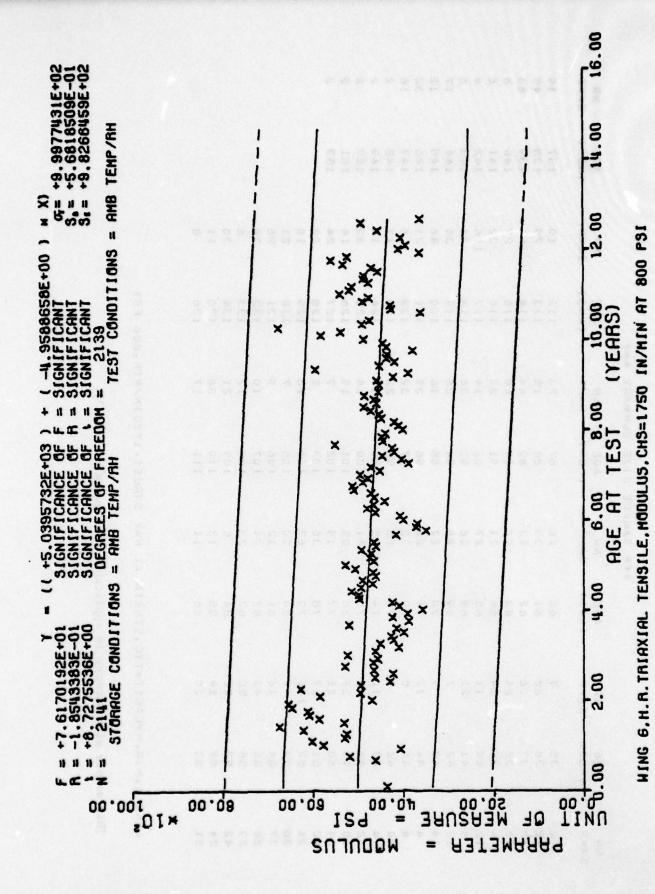
- 31 -





WING 6.H.R.TRIRXIAL TENSILE, STRAIN AT RUPTURE, CHS=1750 IN/MIN, 800 PSI



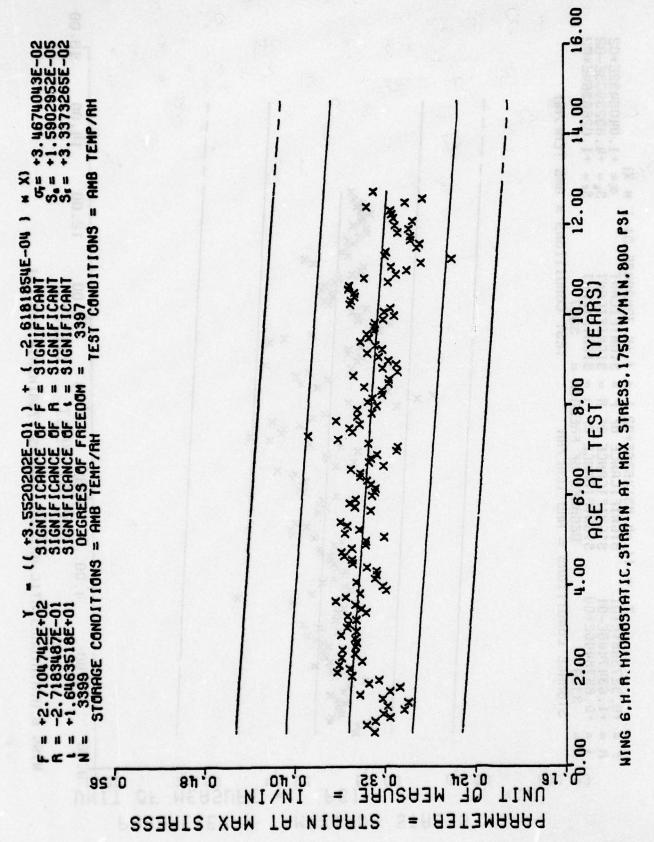


** SAMFLE SIZE SUMMARY ***

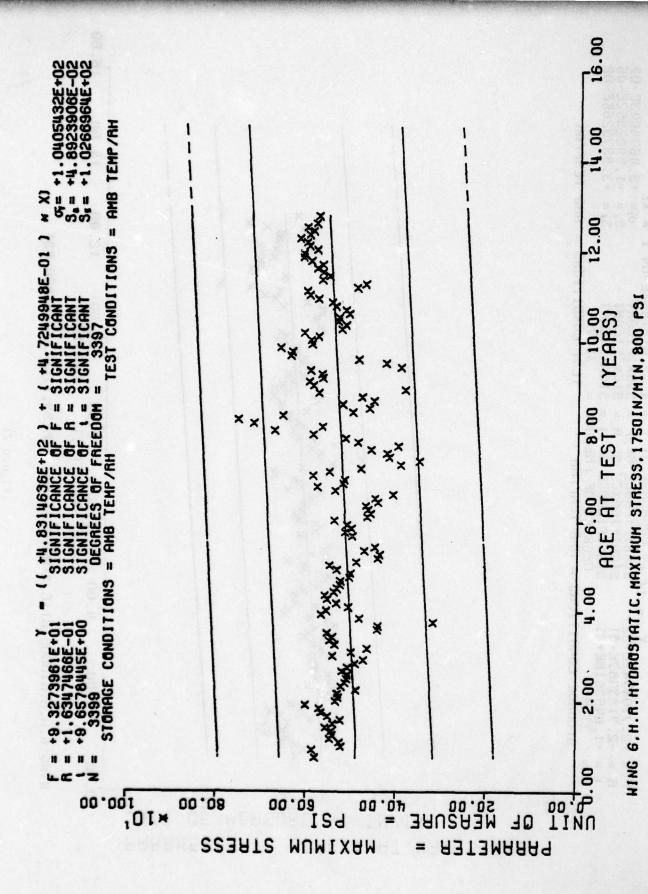
	NR AGE	POSI SAMP (MOSI SAVE	10 137	79 138	139	27 140	32 141	116 142	31 143	34 144	46 145	21 146	9	17 148	14 149	32 150	14 151	24 153	26							
	R.	SAMP	23	15	:	48	23	=	26	26	91	25	32	23	1.7	**	61	7	40	16	7	O.	01	12	21	
	AGE	(KOS)	87	88	68	06	15	92	63	46	95	95	97	86	65	100	101	102	103	104	1 05	901	107	108	601	
SANGET ES	N.	SAVP	56	33	62	100	3.1	27	26	52	27	26	25	65	45	1.	59	51	36	63	50	. 21	24	23	v	
	AGE	(804)	9	19	62	63	99	65	68	69	7.0	7.1	72	73	74	75	92	77	7.8	52	90	18	82	83	84	
	Z.	SAND	,	26	26	54	34	=	12	1	1	15	w	u	10	•	26	26	57	100	64	91	43	50	(5)	
	AGE	(80%)	35	36	37	36	39	0.4	:	42	# 3	44	45	46	47	₩ 4	54	90	51	62	53	50	55	99	57	
	N.	SAMP	2	12	12	91	•	12	80	12	*-	4	•	24		~	91	24	12	31	20	37	28	53	42	
	AGE	NCS)	u	=	12	13	-	15	91	17	82	19	50	21	25	23	54	28	97	27	28	52	30	31	(4)	

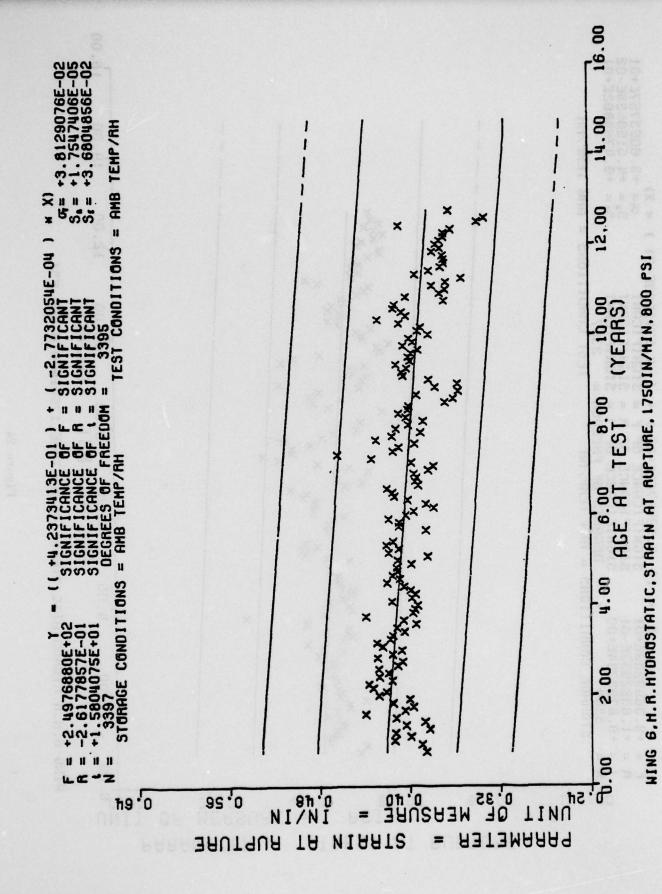
WING 6.4.6.HYCFCSTATIC.STRAIN AT MAX STRESS. 17501N/PIN.600 FSI

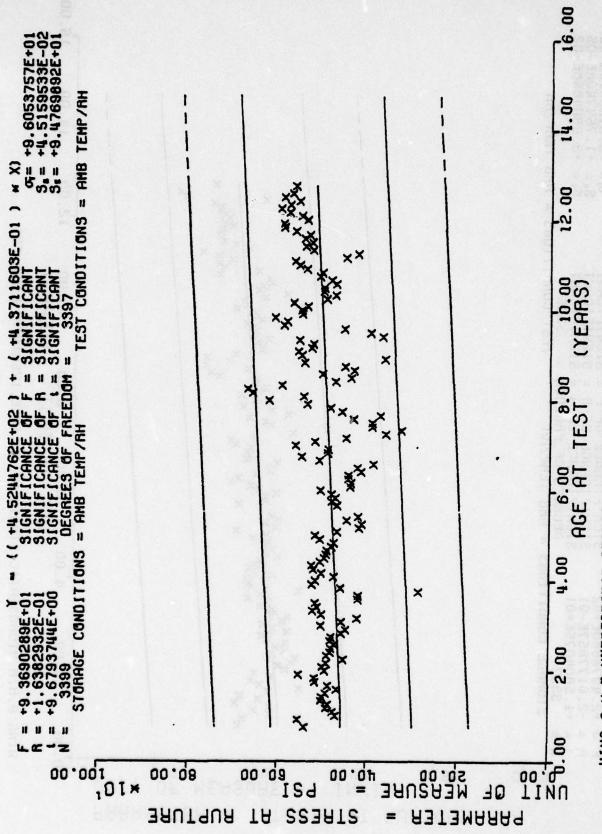
This sample size summary is applicable to figures 21 thru 25.



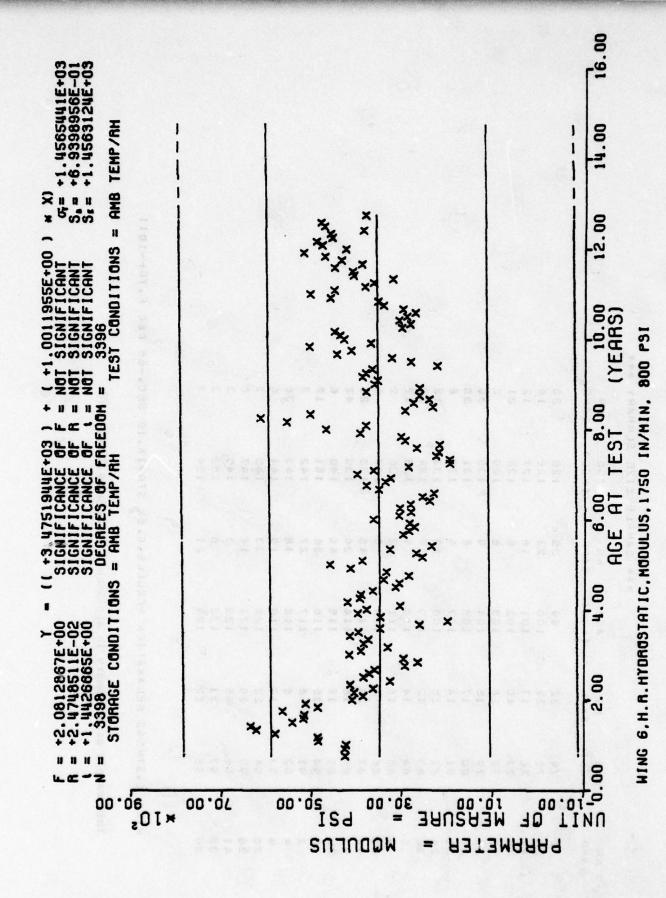
- 37 -







HING 6.H.R.HYDROSTATIC, STRESS AT RUPTURE, 1750IN/HIN, 800 PSI

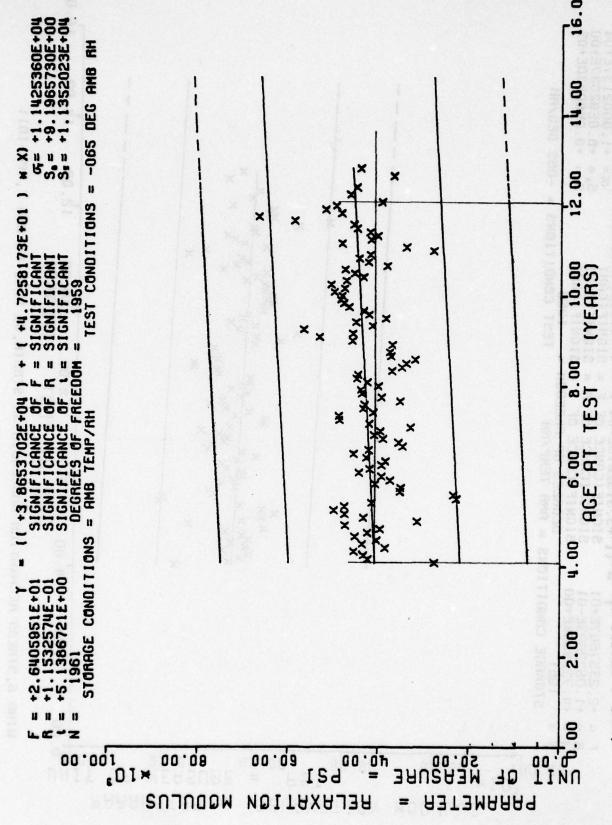


** SAMFLE SIZE SLMMARY ***

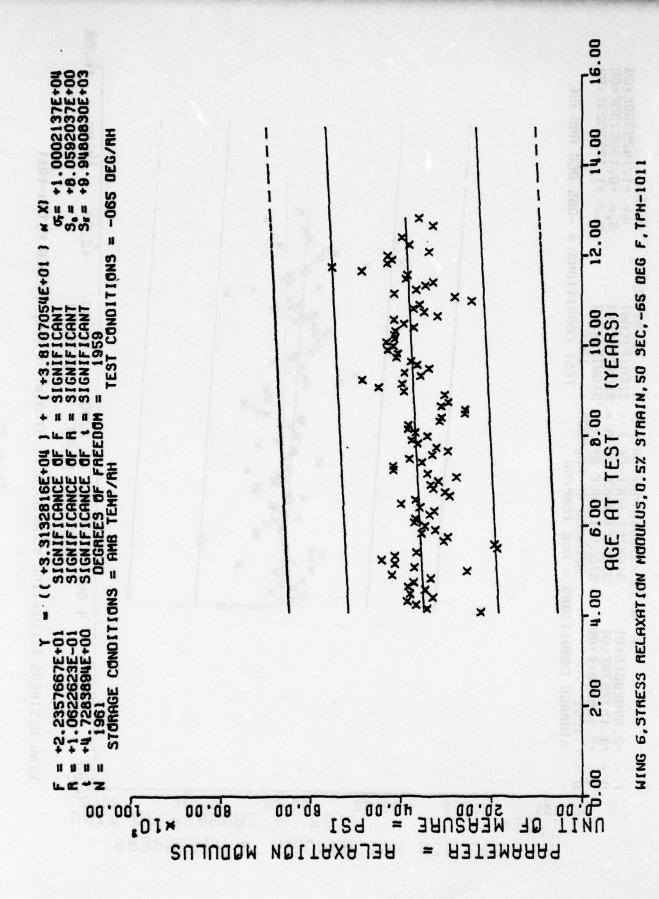
8 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	AGE	E 4	AGE	S A R	AGE	S A S		
	74	35	66	35	125	20		
	75	35	100	23	126	16		
		1.7	101	16	127	12		
	11	9.	102	W)	128	21	2	
	78	26	103	v	129	a		
	52	15	104	σ	130	36		
	80	1.1	105	v	131	30		
	18	:	101	U.	132	w		
	62	()	108	12	133	12		
	83	12	109	12	134	19		
	84	=	110	5	135	31		
	80	1.5	111	m	136	CV		
	98	•	112	Ð	137	9		
	87	24	113	4.5	138	26		
	98	91	114	30	139	45		
	58	16	116	9 C	140	9		
	05	15	116	36	141	12		
	15	9	117	27	142	m		
	95	5	118	18	143	36		
	63	51	611	61	144	v		
	46	23	120	33	145	m ×		
	56	50	121	1.6	147	v		
	96	4.0	122	m	149	m		
	26	61	123	9	152	e		
	96	£2	124	1 2	154	m		

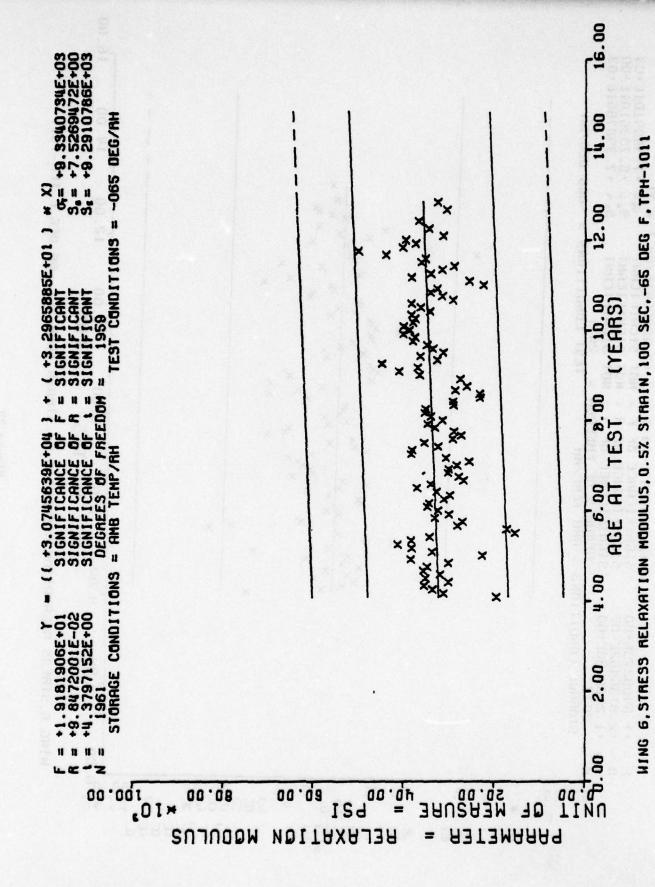
WING C.STRESS RELAXATION MCCULLS. G. 5% STRAIN, 10 SEC. - 65 CEC F. TPF-1011

This sample size summary is applicable to figures 26 thru 29.

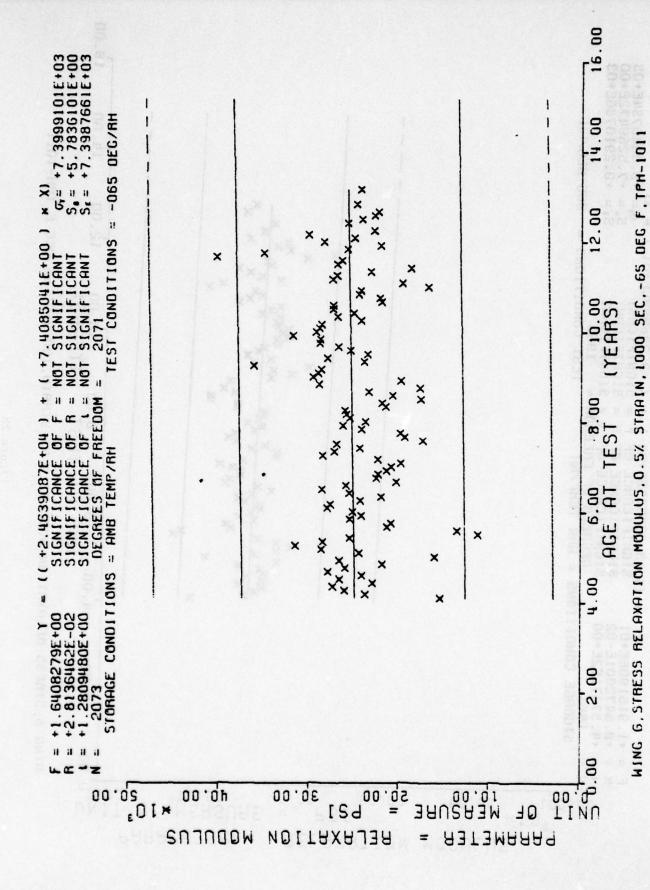


WING 6, STRESS RELAXATION MODULUS, 0.5% STRAIN, 10 SEC, -65 DEG F, TPH-1011





- 45 -

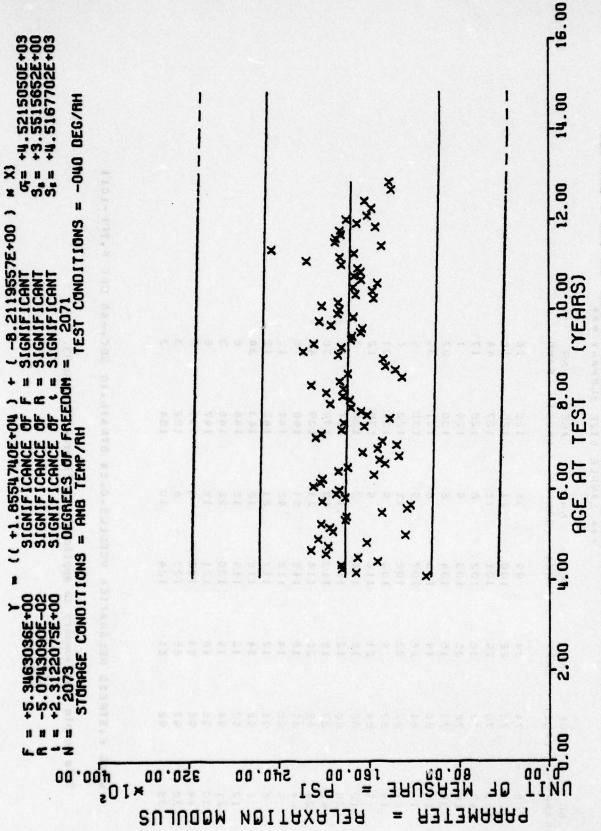


*** SAMPLE SIZE SUMMARY ***

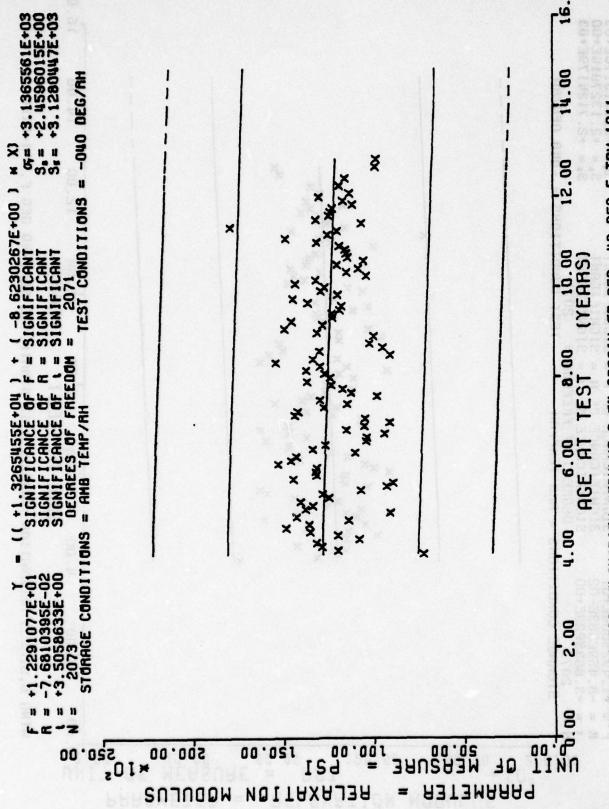
æ	SAME	16	91	:	17	-	27	36	.	¥	31	12	E)	12	36	**	v	12	12	34	¥	ľ	v	(7)	m	ľ")
A GE	(NCS)	126	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	147	149	152	154
Œ	SANE	36	13	16	v	5	¥	w	5	16	5	5	ניז	12	63	12	19	4 (1	1.2	16	91	26	16	E	0 0	16
A GE	(804)	56	100	101	102	103	104	105	101	106	501	011	111	112	113	114	911	116	1117	118	119	120	121	122	123	124
Œ	SANE	34	26	5.2	36	35	97	51	16	61.00	U.	21	31	12	16	20	91	7.	12	24	12	16	16	15	65	£1
AGE	(NOS)	7.4	75	26	11	76	52	96	61	82	83	84	98	96	87	98	88	06	91	25	53	94	50	96	25	96
æ	SANP	v	27	61	47	*	30	18	12	27	51	5	12	20	48	24	24	5	¥	9	12	21	30	44	36	35
AGE	(NCS)	6	0		52	5.5	4.5	41	56	57	Se	C)	9	61	62	1 63	47	. 66	99	67	68	59	20	11	72	73

WING &.STRESS RELAXATION MCCULUS.O. 5% STRAIN. 10 SEC. - 40 DEG F. TPF-1011

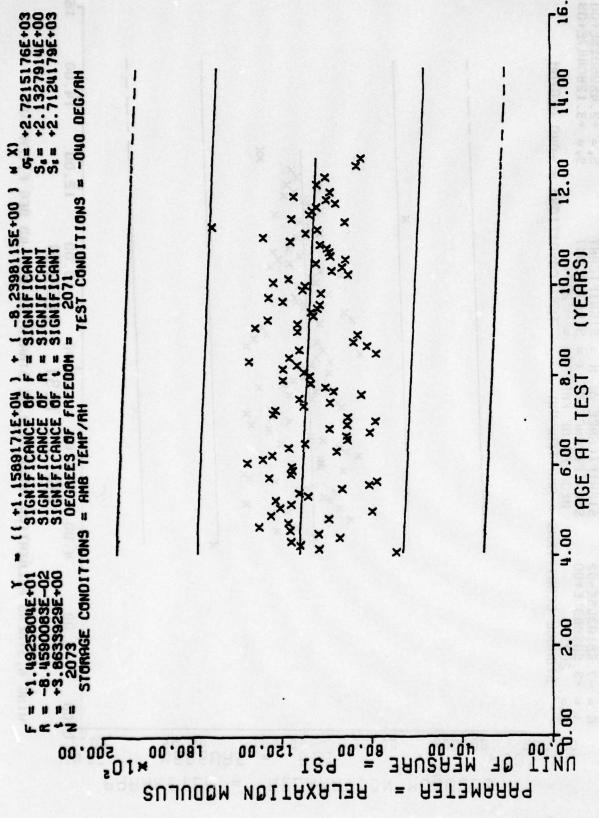
This sample size summary is applicable to figures 30 thru 33.



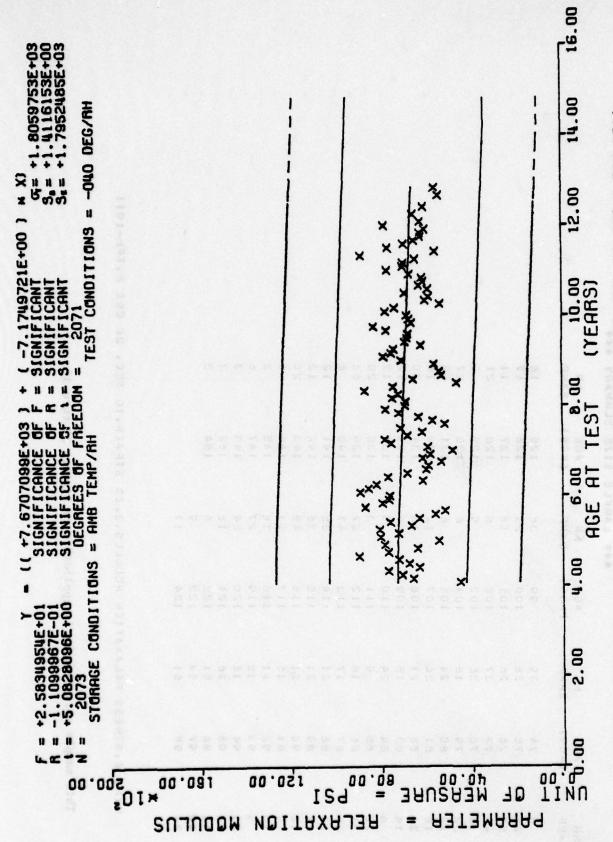
WING 6, STRESS RELAXATION MODULUS, 0.5% STRAIN, 10 SEC, -40 DEG F, TPH-1011



WING 6, STRESS RELAXATION MODULUS, 0.5% STRAIN, SO SEC, -40 DEG F, TPH-1011



WING 6, STRESS RELAXATION MODULUS, 0.5% STRAIN, 100 SEC, -40 DEG F, TPH-1011



- 51 -

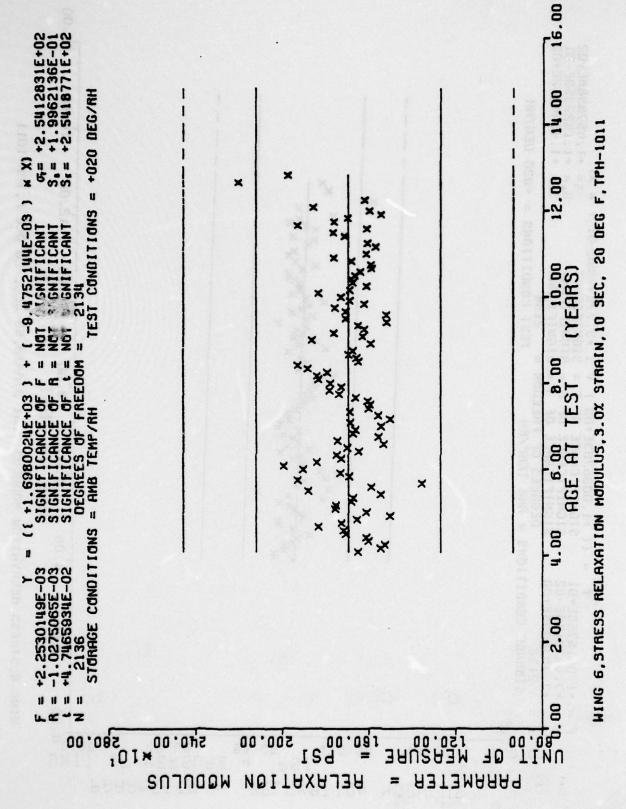
WING 6, STRESS RELAXATION MODULUS, 0.5% STRAIN, 1000 SEC, -40 DEG F, TPH-1011

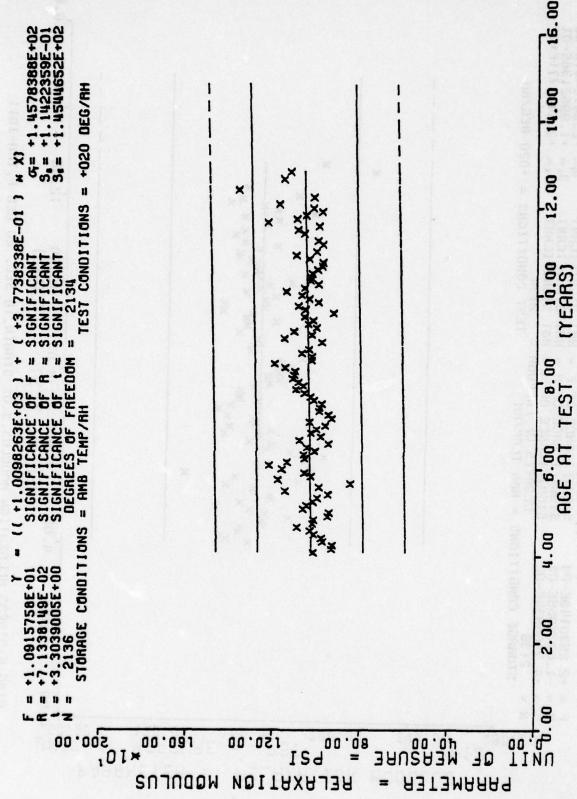
*** SAMFLE SIZE SLMMARY ***

œ 2	SANF	16	17	=	21	m	27	42	16	30	12	12	20	63	v	12	12	20	•	۳)	9	m	m	ניו			
A GE	(804)	125	126	127	128	129	130	131	132	134	135	137	138	138	140	141	142	143	144	145	147	149	152	154			
E.	SANE	36	21	1.6	'n	5	v	¥	12	. 51	•	6	E	27	47	U) (7)	36	45	2.1	1.6	27	24	16	9	5	17	
AGE	(804)	66	100	101	102	103	104	105	101	801	109	110	111	112	113	114	116	116	1117	118	611	120	121	122	123	124	
N.	SANE	35	36	26	37	36	1.8	72	30	27	16	24	5	16	17	21	21	21	31	21	9	16	56	19	40	-	
AGE	(804)	74	75	76	77	7.6	52	90	18	82	83	84	65	86	18	88	58	06	16	82	93	45	96	96	25	98	
œ.	SANP	•	27	60	9.7				18			•	22	21	54	24	27	12	5	01	5	58	24		42		
AGE	MCS)	54	20	19	52	53	+ 5	w)	99	67	36	5	09	61	62	63	19	65	99	67	99	69	70	17	72	73	

WING C.STRESS RELAXATION MOCULUS.3.CX STRAIN.10 SEC. 20 DEG F.TPH-1011

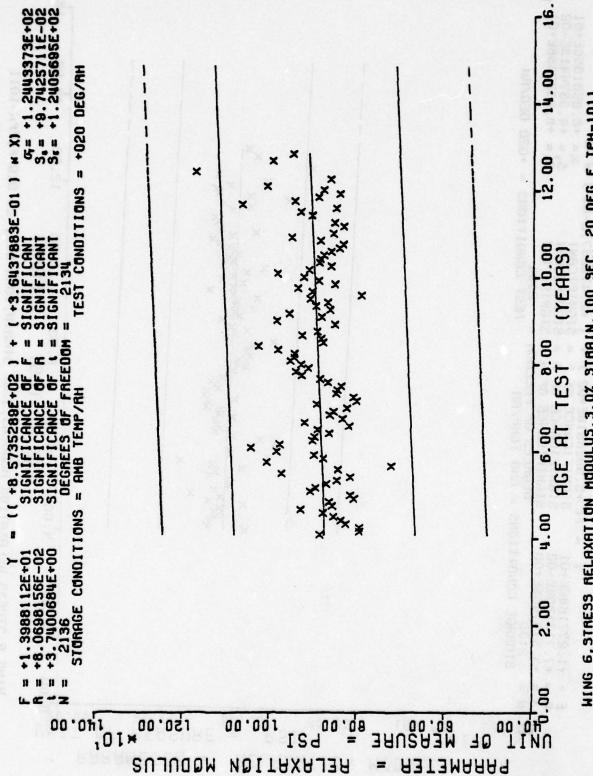
This sample size summary is applicable to figures 34 thru 37.



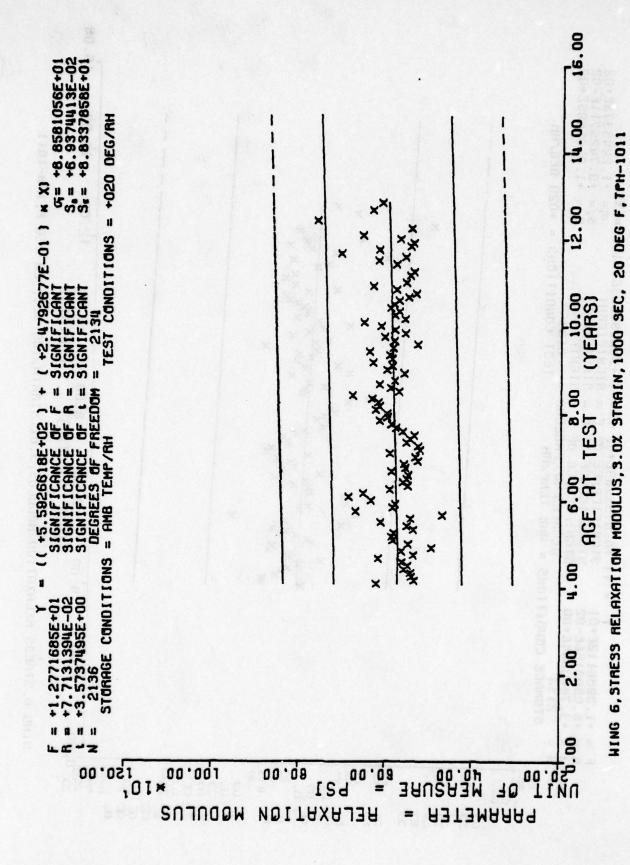


- 54 -

WING 6, STRESS RELAXATION MODULUS, 3.0% STRAIN, 50 SEC, 20 DEG F, TPH-1011



WING 6, STRESS RELAXATION MODULUS, 3.0% STRAIN, 100 SEC, 20 DEG F, TPH-1011



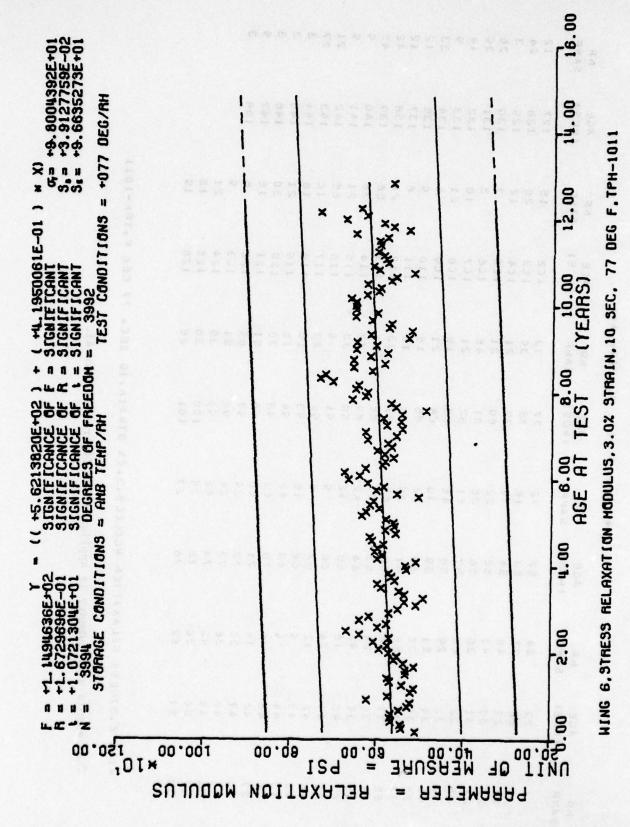
- 56 -

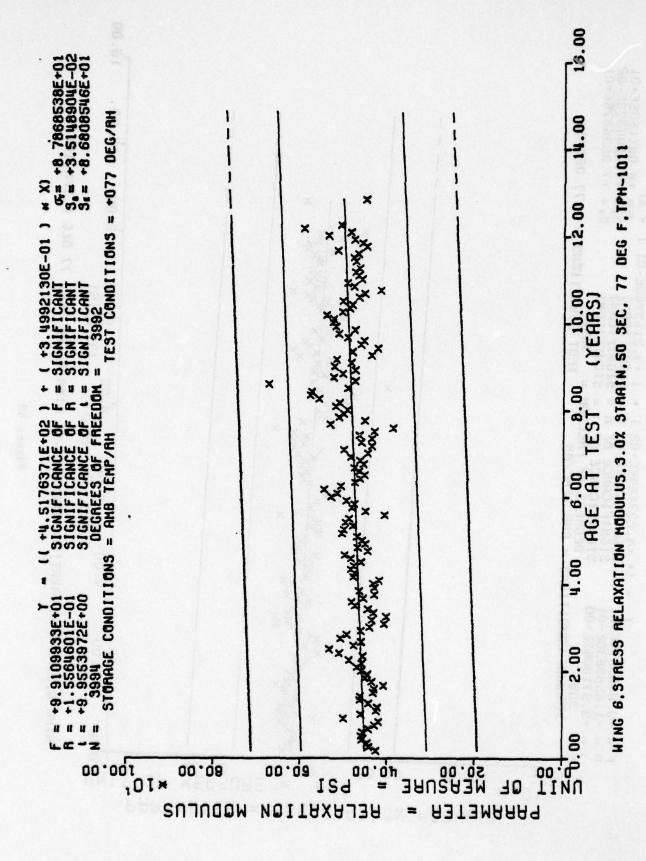
*** SAMFLE SIZE SUMMARY ***

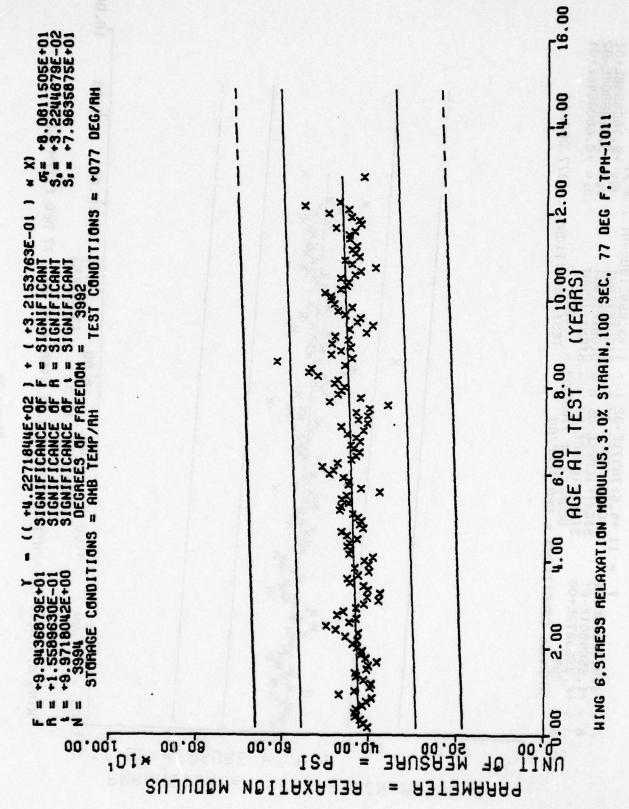
1 4 W	15	54	m	36	38	=	•	33	12	12	. 45	-	•	0		27	m	m	m	•	m				
(NOS)	127	128	125	130	131	132	133	134	135	137	138	139	140	==	142	143	:	145	941	147	154				
SAME	1.5	20	15	9	r)	01	21	v	6	9	21	56	38	21	65	91	91	21	30	6 7	•	•	12	91	1.0
(PCS)	102	103	104	105	106	107	108	501	110	111	112	113	***	115	116	117	118	119	120	121	122	123	124	125	701
SAMP	33	36	21	21	4	21	15	12	15	16	33	12	27	33	us.	23	51	16	30	15	59	19	35	20	9
(POS)	11	78	52	90	18	82	63	84	85	96	18	68	689	05	816	92	63	96	95	95	25	96	65	100	101
SAMP	7.2	18	36	22	36	61	46	30	56	39	65	27	42	12	5	9	91	42	63	33	52	24		5:2	2.2
(804)	52	63	54	w w	99	57	58	55	09	61	62	63	64	65	99	67	68	69	7.0	7.1	72	73	74	75	76
A 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	24	27	46	4.3	36	9	52		36			24						v.	9	16	30	36	42	36	
(804)	27	26	25	30	31	32	33	34	35	36	37	36	36	9	4.1	42	4 3		45	46	47	4 6	54	20	
SARP	•	•		22	21		30	45	36	37	65	51	46	57	36	46	13	10	•	27	5	y	34	27	30
MCS)	(V	")	•	u,	v	1	w	5	91	11	12	13	-	15	91	71 1		19	20	21	22	23	24	25	26

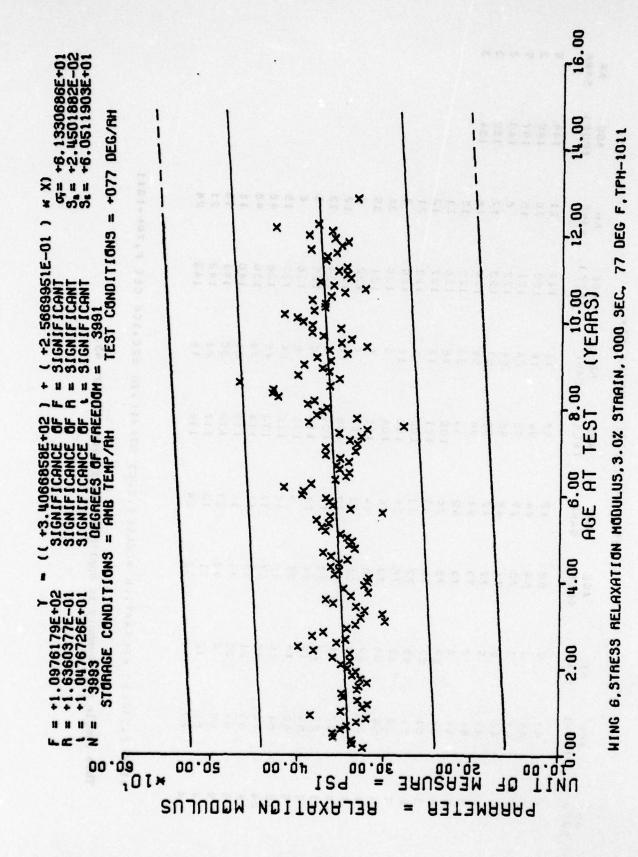
WING C.STRESS FELAXATICN MCCULLS.3.CX STRAIN.10 SEC. 77 DEC F.TPF-1011

This sample size summary is applicable to figures 38 thru 41.







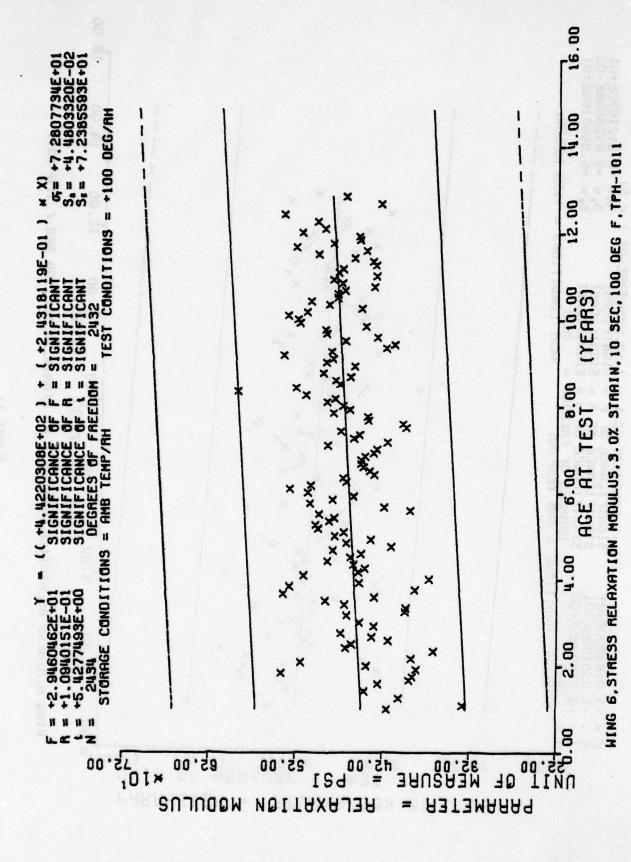


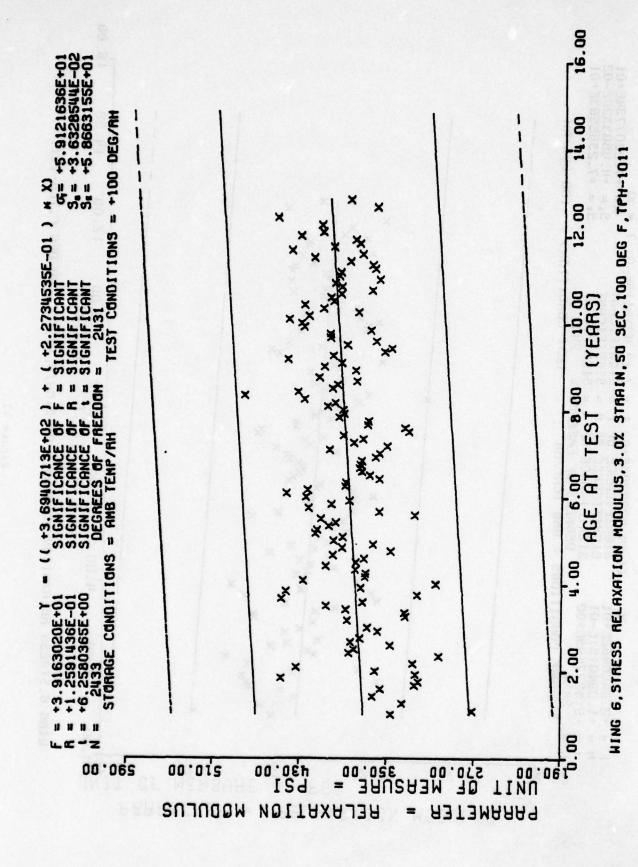
*** SAMFLE SIZE SLMMARY ***

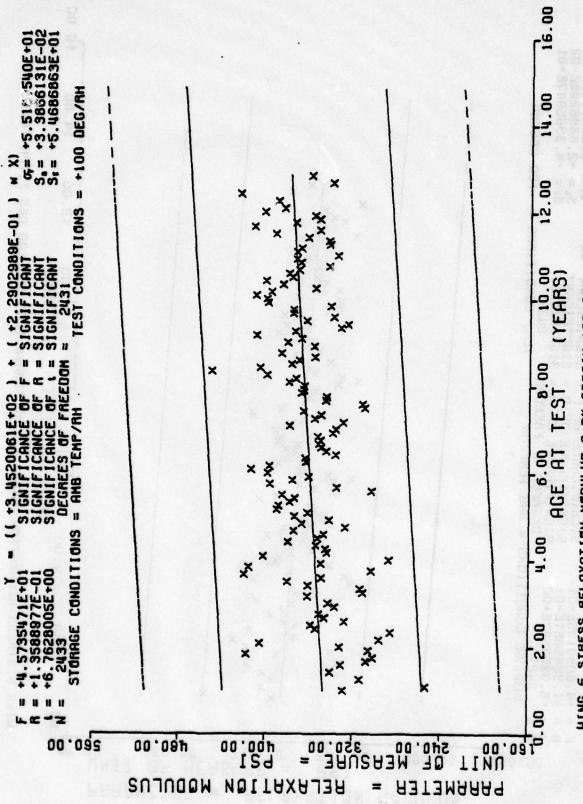
4	SANE	•	r)	5	")	"	9																			
AGE	(SDM)	144	145	147	149	152	154																			
3	SANE	12	36	15	w	12	91	16	21	12	21	Ю	36	36	o,	12	33	5	¥	15	46	46	16	91	21	24
AGE	(814)	611	120	121	122	123	154	125	126	127	128	125	130	131	132	133	134	125	136	137	138	139	140	141	142	143
Z Z	SANE	16	16	54	5.4	53	5.4	36	16	31	U.	15	5	ų	¥	31	ø	5	9	24	9 6	38	2.1	30	21	1.6
A GE	(SDA)	53	76	35	9.ç	25	96	66	100	101	102	1 63	104	105	107	108	501	110	1111	112	113	114	115	911	117	116
œ	SANE	12	54	23	46	4.2	24	42	36	53	33	3.6	31	24	(")	2.7	1 8	213	6	16	12	11	16	27	12	24
AGE	(SDA)	6.8	59	10	7.1	72	7.3	7.4	7.5	16	77	7.8	7.9	08	9.1	32	63.3	94	95	æ	87	896	e e	06	31	25
7.	SANE	O,	ייו	55	9	v	ניו	y	27	57	4 €	12	93					12						ΰ	12	ý
AGE	(NOS)	4 5	44	4	46	47	4 E	54	50	51	(2)	נח נט	54	נוי נוי	36	57	e)	5.5	90	61	62	63	6.4	ć, S	ĢĆ	67
7	SAMP	m	17)	•	- 2	v	6	5	¥	۳	e	5	c	(2)	5	5	ריז	5	5		24		()	5	12	•
AGE	MCSD	12	13	1.5	11	15	20	21	22				25												41	42

WING 6.STRESS RELAXATION MCCLLUS.3.C% STRAIN.10 SEC.100 DEG F.TPF-1011

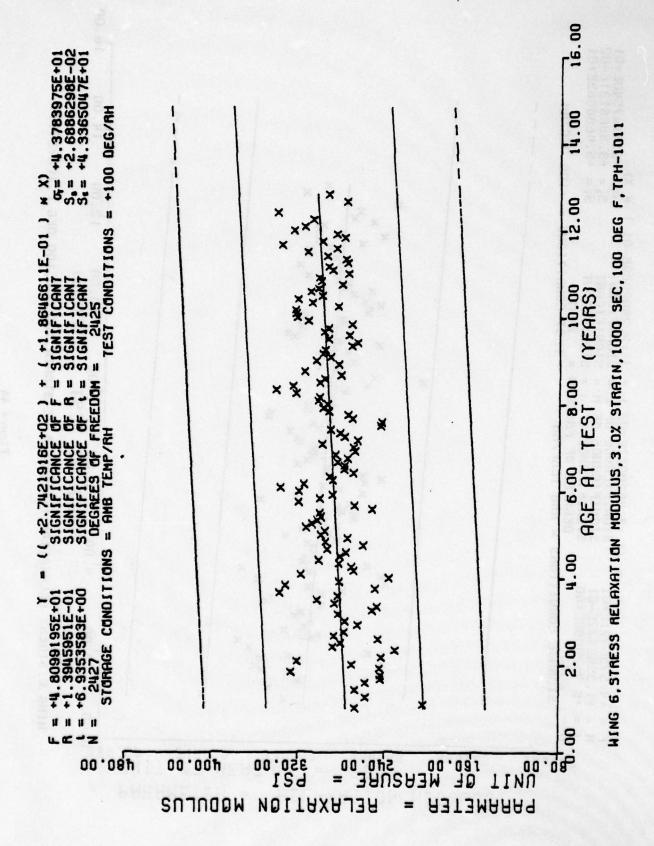
This sample size summary is applicable to figures 42 thru 45.







WING 6. STRESS RELAXATION MODULUS, 3.0% STRAIN, 100 SEC, 100 DEG F. TPH-1011



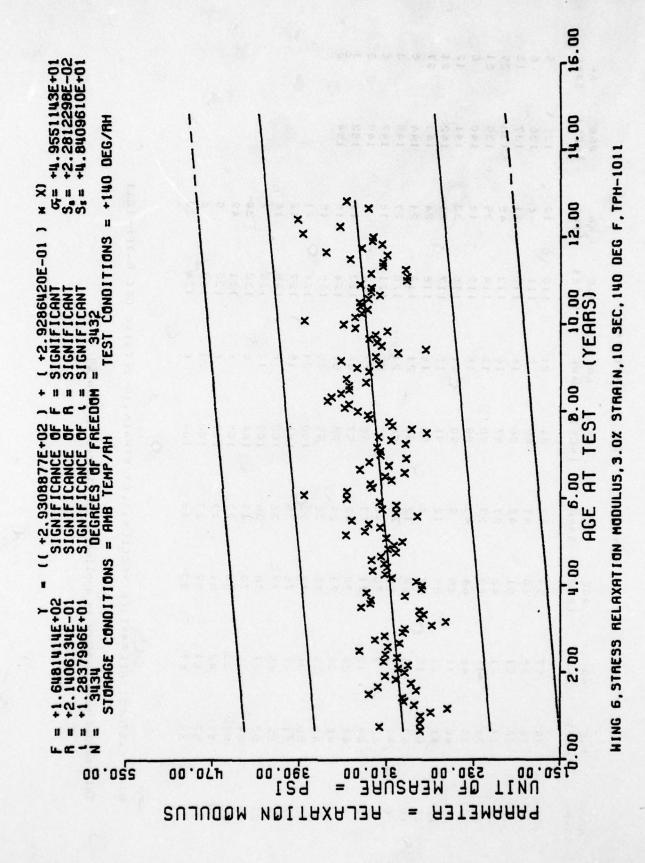
- 66 -

*** SAMPLE SIZE SLMMARY ***

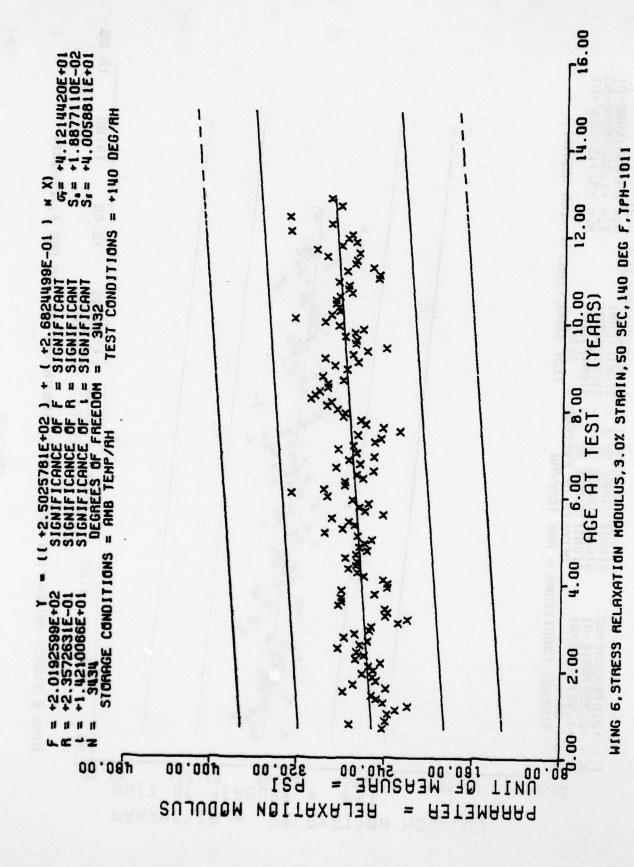
SAMP (MUS) SAMP (MCS) SAMP (MCS) SAMP (MCS) 4 27 53 33 64 21 110 12 136 6 60 47 65 67 67 67 111 6 136 7 21 62 67 67 67 16 112 46 136 9 16 64 45 69 16 116 33 141 1 21 16 116 116 33 141 2 16 16 116 33 141 2 16 16 116 33 141 2 16 16 116 33 141 2 16 16 21 16 144 3 17 46 96 21 116 144 4 6 46 96 20 121 <th>39¢</th> <th>12 /</th> <th>AGE</th> <th>4</th> <th>₽ GE</th> <th>A.R.</th> <th>AGE</th> <th>A A</th> <th>AGE</th> <th>7</th>	39¢	12 /	AGE	4	₽ GE	A.R.	AGE	A A	AGE	7
6 59 33 84 21 110 12 136 6 6 47 65 6 41 65 6 111 6 136 137 136 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 137 138 138 139 139 138 139 139 139 139 139 139 139 139 130 130 130 130 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140	(80A)	2	(NUS)	SANF	(804)	SANE	(PCS)	SARR	(NCS)	SANE
5 5 6 41 65 9 111 6 136 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 137 13 6 130 13 140 13 140 6 140 6 140 6 140 6 140 6 140 6 140 6 140 140 6 140 140 6 140 140 140 6 140 140 6 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140 140 1			60		48	21	110	12	136	5
E E E I 48 BC IC II 45 I39 35 I39 36 1 1 6 4 4 6 1 1 4 139 35 139 35 139 36 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			60		85	5	111	w	136	•
7 21 62 67 67 11 113 46 136 136 136 136 139 6 140 141 140 140 140 140 140 140 141 140 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141 141			61		8¢	91	112	12	137	15
36 16 63 27 96 12 114 39 139 5 35 46 64 46 69 16 116 18 140 40 16 12 16 116 21 140 41 21 66 12 90 21 140 141 42 16 12 92 16 117 21 140 24 144 44 44 44 44 46 93 21 116 144 44 144 44 44 47 46 94 21 120 27 144 44 44 46 94 21 120 27 144 44 46 46 95 20 121 140 46 46 96 57 122 6 140 46 46 96 57 123 6 140 46 46 96 57 <td>(1)</td> <td></td> <td>62</td> <td></td> <td>87</td> <td>1.6</td> <td>113</td> <td>4.5</td> <td>138</td> <td>35</td>	(1)		62		87	1.6	113	4.5	138	35
35 46 64 46 89 16 116 33 141 1 40 16 12 90 21 116 33 141 1 41 21 66 12 91 12 16 142 24 143 2 45 69 46 92 16 117 21 144 2 144 2 144 4 4 4 4 6 9 20 16 117 21 144 4 4 4 6 9 20 16 144 4 144 4 4 6 9 20 16 144 4 144 4 6 9 20 16 147 4 6 149 9 149 9 149 9 149 9 149 9 149 9 149 149 149 149 149 140 140	(*)		63		98	12	114	36	139	13
4C 1E 65 9 21 116 33 141 1 41 21 66 12 91 15 117 21 142 2 42 16 12 93 21 119 24 143 2 44 9 69 46 94 21 120 27 144 2 144 20 144 20 144 20 144 20 27 145 20 145 20 145 20 145 20 145 20 145 20 145 20 145 20 145 20 145 20 145 20 145 20 145 46 46 50 50 50 123 140 140 140 140 46 46 50 50 150 60 150 150 150 150 160 150 150 160 150	n		64		68	16	115	9.1	140	9
41 21 66 12 91 15 117 21 142 2 42 16 63 68 12 93 21 118 24 143 8 44 9 69 46 92 16 116 118 24 143 8 45 9 46 8 9 20 121 144 145 145 4 145 4 145 4 145 145 145 145 145 4 145 145 145 145 145 4 145 145 145 145 145 145 145 145 145 145 145 145 145 145 145 145 145 145 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 <t< td=""><td>4</td><td></td><td>ćS</td><td>o</td><td>06</td><td>21</td><td>116</td><td>33</td><td>141</td><td>12</td></t<>	4		ćS	o	06	21	116	33	141	12
42 16 67 6 92 16 116 24 143 8 43 5 68 12 93 21 119 21 144 44 9 69 46 94 81 120 27 145 45 3 70 46 95 20 121 144 147 46 12 95 20 121 16 147 145 145 145 147 146 147 146 147 146 147 146 147 146 147 146 147 146 147 146 147 146 147 147 146 147 146 146 147 146 146 147 146 146 146 146 146 146 146 146 146 146 146 146 146 146 146 146 146 146 146 146	4		99	12	15	16	117	2.1	142	21
43 5 68 12 93 21 119 21 144 44 5 69 46 54 21 120 27 145 46 12 95 20 121 16 147 46 12 96 57 122 6 149 47 30 72 42 96 51 12 149 46 36 73 24 96 51 12 15 15 45 36 74 36 96 51 12 154 15 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 154 <td></td> <td></td> <td>57</td> <td>w</td> <td>85</td> <td>1.6</td> <td>116</td> <td>24</td> <td>143</td> <td>27</td>			57	w	85	1.6	116	24	143	27
44 9 69 46 94 21 120 27 145 46 12 20 121 12 147 46 12 20 121 16 147 47 30 72 42 96 57 152 6 47 36 73 24 98 51 12 16 165 45 36 74 36 96 51 154 15 154 16 154 154 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165 165	4		c, &		63	21	119	21	144	•
45 3 70 46 95 20 121 16 147 46 12 71 67 65 57 162 6 149 47 30 72 42 97 56 153 16 149 46 36 73 24 98 51 124 15 154 47 36 74 36 101 15 126 21 50 36 101 15 126 21 51 6 77 36 103 12 129 2 53 27 78 36 103 12 129 2 54 36 103 12 129 2 55 33 106 6 130 30 56 33 107 6 133 6 56 32 107 6 133 6 57 51 108 21 134 33	4	ဟ	69	46	45	2.1	120	27	145	6
46 12 71 €7 56 57 152 € 149 47 30 72 42 97 56 153 12 152 46 36 73 24 98 51 124 16 154 16 154 16 154 16 154 15 154 15 154 15 154 15 154 15 154 15 154 16 154 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16	4	E	7.0	4.5	95	20	121	× 16	147	v
47 30 72 42 97 56 153 12 152 46 35 73 24 98 51 124 16 154 45 35 74 36 39 39 125 15 50 36 75 35 100 21 126 21 51 6 76 36 101 18 127 18 52 6 77 36 103 12 129 2 53 27 78 36 103 12 129 2 54 30 23 106 6 130 30 55 42 81 27 107 6 133 6 56 42 83 13 109 6 134 33	4	12	1.2	67	95	57	122	•	149	"
E 35 74 36 98 51 124 15 154 9 35 74 36 39 39 125 15 1 6 75 32 100 21 126 21 2 6 76 36 101 16 12 12 3 27 78 36 103 12 129 2 4 3C 79 17 104 6 130 30 6 42 80 23 107 6 131 42 7 51 107 6 133 6 42 8 27 108 21 133 6 8 57 109 6 134 33	4	30	72	42	25	56	123	12	152	3
9 36 74 36 39 39 125 10 1 6 75 32 100 21 126 2 2 6 77 36 101 16 127 1 3 27 78 36 103 12 129 1 4 3C 79 17 104 6 130 3 6 42 81 27 107 6 131 4 7 51 82 27 108 21 133 8 57 83 13 6 134 3		5:7	73	54	96	51	124		154	(*)
0 36 75 32 100 21 126 2 1 6c 76 36 101 16 127 1 2 65 77 36 102 6 128 1 3 27 78 36 103 12 129 1 4 3C 79 17 104 6 130 3 6 42 81 27 107 6 132 4 7 51 82 27 108 21 133 8 57 83 13 6 134 3		517	74	300	55	50	125			
1 66 76 36 101 15 127 1 2 65 77 36 102 6 128 1 3 27 78 36 103 12 129 1 4 3C 79 17 164 6 130 3 6 42 81 27 167 6 132 4 7 51 82 27 108 21 133 8 57 83 13 13 3		36	75	r) r)	100	21	126			
2 65 77 36 102 6 128 1 3 27 78 36 103 12 129 4 3C 79 17 164 6 130 3 6 33 80 23 167 6 131 4 6 42 81 27 167 6 132 7 51 83 13 109 6 134 3		ć.ć	76	36	101	31	127			
3 27 78 36 103 12 129 4 3C 79 17 104 6 130 3 6 33 80 23 105 6 131 4 6 42 81 27 107 6 132 7 51 82 27 108 21 133 8 57 83 13 6 134 3		53	77	in in	102	w	128			
4 2C 79 17 1C4 6 130 3 5 33 80 23 1CF 6 131 4 6 42 81 27 1C7 6 132 7 51 82 27 108 21 133 8 57 83 13 6 134 3		27	78	36	103	12	129	2		
6 33 80 23 105 c 131 4 6 42 81 27 107 6 132 7 51 82 27 108 21 133 8 57 83 18 109 6 134 3		30	23	17	104	Ų	130			
6 42 81 27 107 6 132 7 51 82 27 108 21 133 8 57 83 18 109 6 134 3		ניו ייי	80	17)	105	u	131			
7 E1 82 27 108 21 133 8 E7 83 18 109 6 134 3		42	81	27	107	v	132	G		
8 67 83 18 109 6 134 3		6.1	82	27	108	21	133	v		
		57	83	13	501	v	134			

WING 6.STRESS RELAXATION MCCLLUS, 3. CX STRAIN, 10 SEC. 140 DEC F. TFF-1011

This sample size summary is applicable to figures 46 thru 49



- 68 -



- 69 -

- 70 -

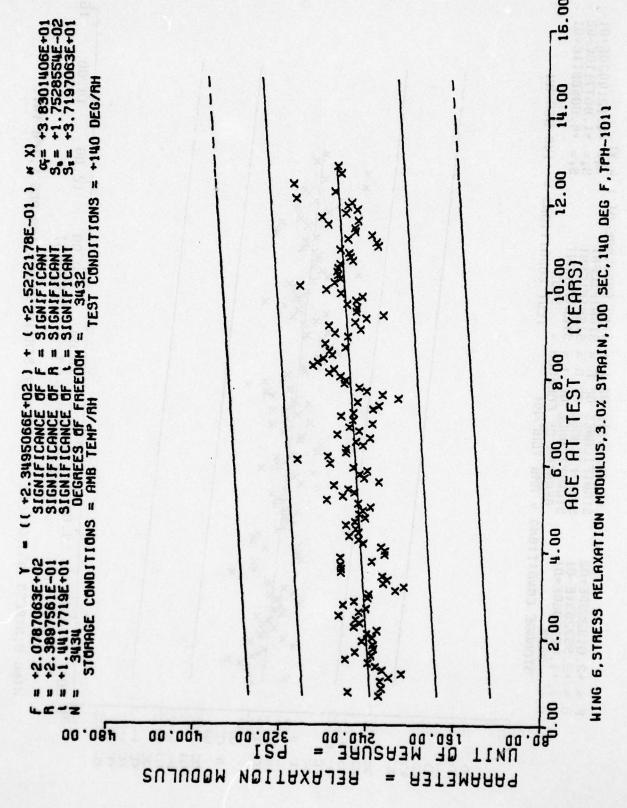
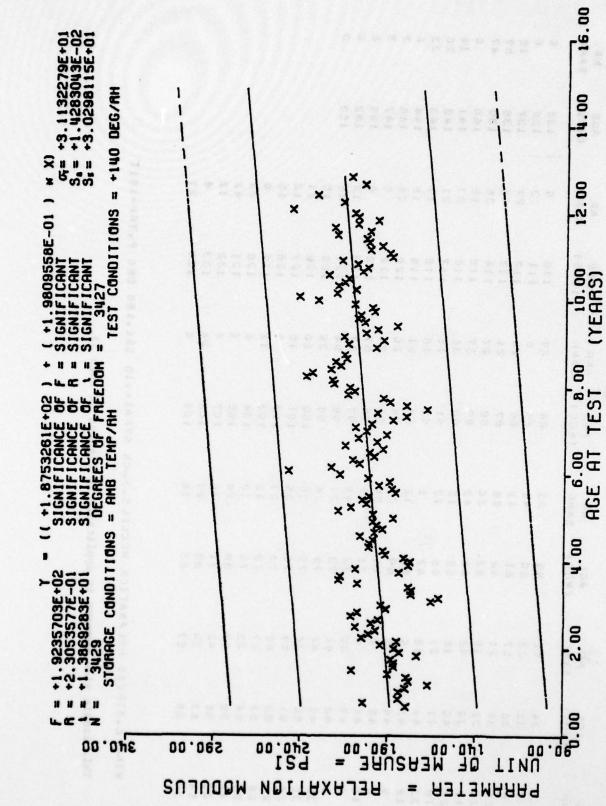


Figure 48



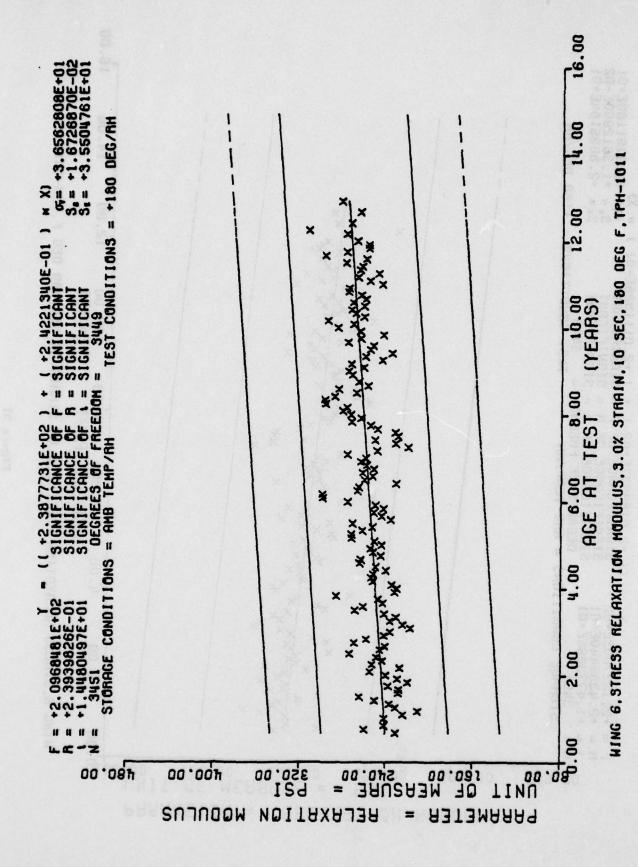
WING 6, STRESS RELAXATION MODULUS, 3.0% STAAIN, 1000 SEC, 140 DEG F, TPH-1011

** SAMPLE SIZE SLMMARY ***

ų.	SANE		•	31	57	47	9	15	50	(n) (n)	.	(*)	m	•	~	m						**		1"		
AGE	(SDM)	136	136	137	136	139	140	141	142	143	144	146	147	149	152	166										
Z.	SANE	•	6	27	46	36	16	33	21	17	91	26	· ·	v	12	15	91	21	12	91	v	24	42	12	w	21
AGE	(PCS)	110	1111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134
X	SAKE	24	v	16	12	27	27	36	16	16	21	50	21	57	57	54	38	20	92	u	12	v	5	v	24	¥.
A GE	(\$04)	84	es	96	87	88	68	05	15	55	63	45	95	95	97	86	65	100	101	102	103	104	105	101	108	501
Œ	SAME	63	46	42	5.8	30	42	12	12	•	12	39	99	177	46	27	36	36	38	27	42	18	24	90	27	16
A GE	(NOS)	56	09	19	62	63	64	65	99	29	68	69	02	7.1	72	73	74	75	92	11	7.8	62	90	18	82	83
u Z	SAKE	15	63.53	57	51	16	46	16	21	1.8	5	•	y	•	36	42	42	36	57	99	27	33	33	42	43	67
AGE	(NOS)	3.	36	36	37	36	38	90		42	43	44	45	46	47	46	54	90	19	52	53	5.4	55	56	57	58
2	SAMP	m	5	y	24	24	12	24	18	33	16	•	v	16	•		36	38	24	24	26	20	42	33	49	36
AGE	MCS)	w	v.	10	12	13	14	15	16	11	18	15	20	21	14.5	23	24	25	26	27	26	58	30	31	32	33

WING 6.STRESS RELAXATION MCCULLS.3.CX STFAIN.10 SEC.180 DEG F.TFH-1011

This sample size summary is applicable to figures 50 thru 53.



- 73 -

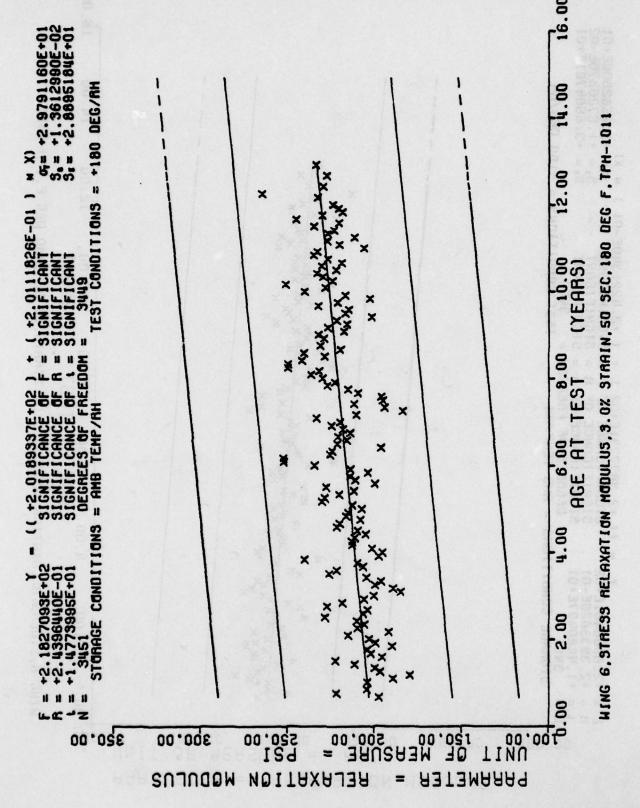
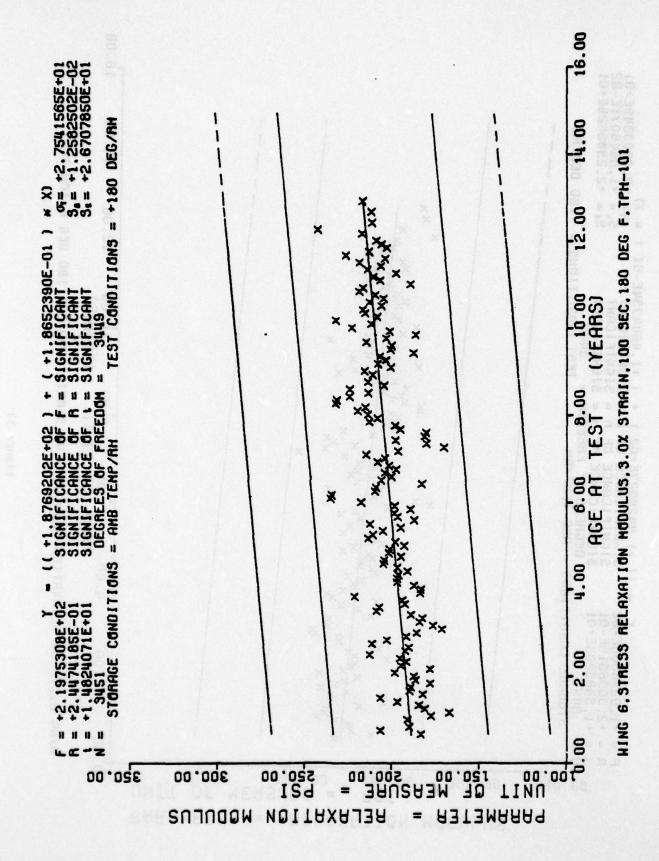
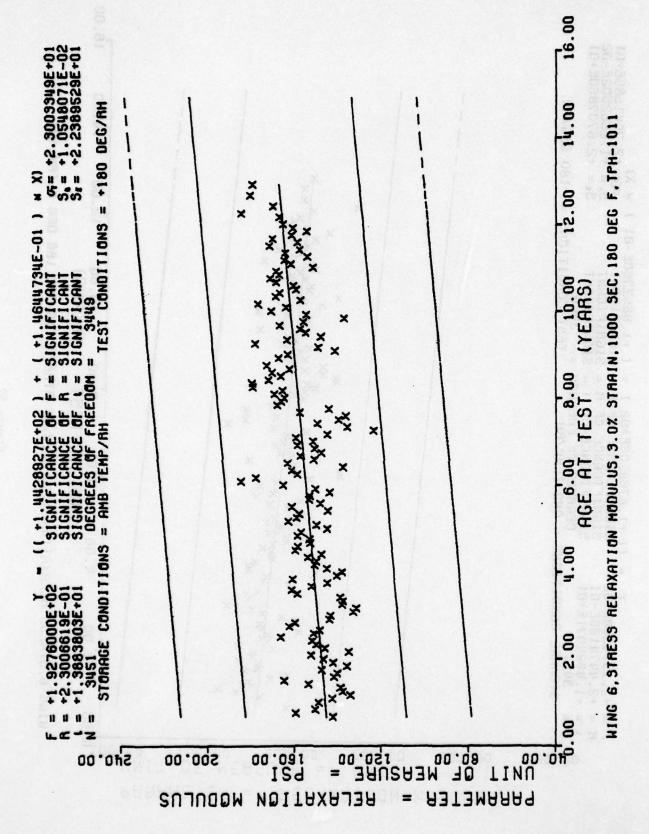


Figure 51





- 76 -

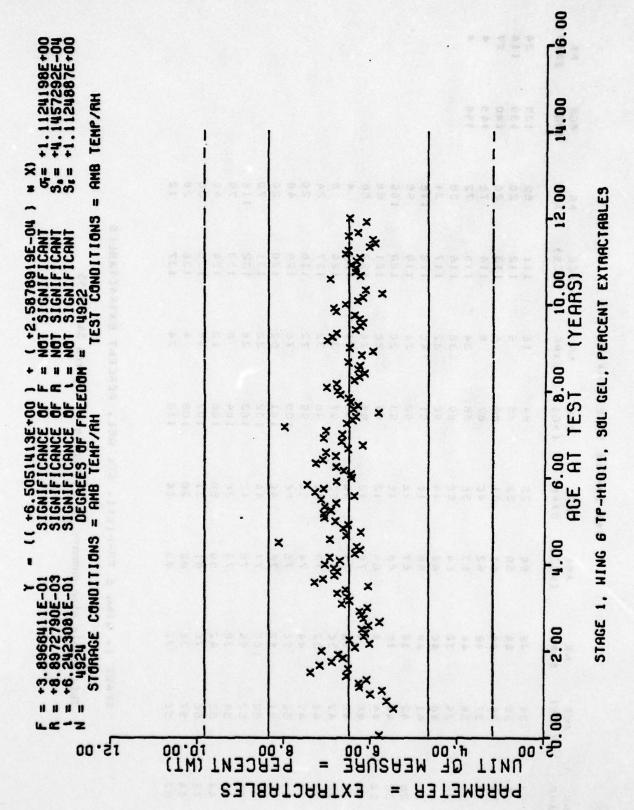
*** SAMFLE SIZE SLMPARY ***

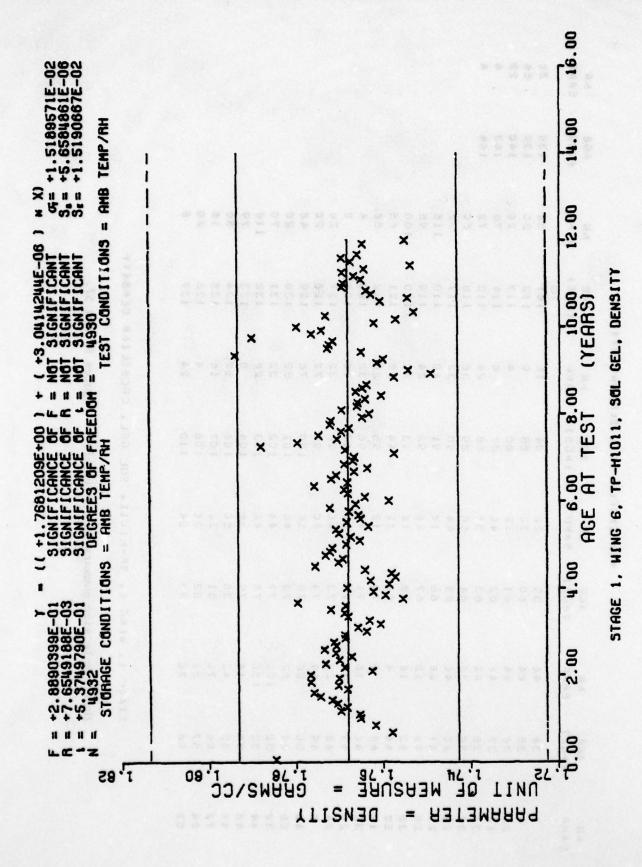
8 P P	P	111	. 27	•							.,	1 1 1 1 1 1 1		!								•		,	
AGE (NOS)	138	139	140	143	**																				
SAR	52	20	20	76	72	56	31	116	80	100	66	99	*	8	24	20	48	20	20	116	42	•	36	26	12
(NCS)	==	112	113	114	115	116	117	811	119	120	121	122	123	124	127	128	129	130	131	132	133	134	135	136	137
SANP	16	5	•	•	24	36	32	40	24	20	28	26	31	36	32	72	76	52	32	28	•	12	16	•	24
(NGS)	84	85	86	18	88	68	05	16	55	65	45	95	95	97	86	56	100	101	102	103	104	901	107	108	110
SAVE	32	2	7,	40	36	56	*	91	26	91	12	12	40	62.8	40	96	56	40	44	42	36	50	3.1	20	24
(NOS)	59	9	19	62	63	64	65	99	67	68	69	7.0	7.1	72	73	74	75	92	11	7.8	79	80	81	82	83
A 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	46	64	;	46	44	(4)	90	2.6	12	16	× • • • • • • • • • • • • • • • • • • •	æ	16	36	32	:	20	52	100	55	36	42		36	26
(NOS)	34	35	36	37	36	36	•	7	42	43	:	*	46	47	46	54	30	51	52	E)	54	20		57	
SAMP	m	•	24	12	32	36	20			32		12	32				0.4		32	44	43	**	72	64	
(MCS)	-	w	10	12	13	*:	51	91	1.7	18	51	20	21	W	2	¥2 77	N	26	27	26	52	36		35	P) 17

STAGE 1. WING 6 TP-FIGII. SCL GEL. PERCENT EXTRACTABLES

This sample size summary is applicable to figures 54 and 55







- 79 -

** SAMFLE SIZE SLMMARY ***

A 46				5	100	3633	1027. 14		100000	9	3	,
2 4 6 5 5 5 6 111 6 111 6 113 2 113 6 113 2 140 143 144 143 144 143 144 143 144 143 144 143 144 144 144 144 145 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144 144	MCS 1	SAMP	(AGS)	4	(NOS)	SAVP	(\$04)	SAKE	(PCS)	SAPE	(MOS)	SAN
6 4 35 64 60 32 85 9 112 20 139 2 12 37 46 61 32 86 4 113 20 149 3 32 34 61 32 86 4 113 20 149 3 36 36 64 66 16 93 24 116 60 144 4 40 63 36 16 69 32 117 32 144 5 20 47 26 93 26 116 60 16 16 93 117 144 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 16 <td>-</td> <td>E</td> <td>34</td> <td>46</td> <td>56</td> <td>ev Pr</td> <td>84</td> <td>16</td> <td></td> <td>22</td> <td>138</td> <td></td>	-	E	34	46	56	ev Pr	84	16		22	138	
24 36 44 61 22 86 4 113 20 144 3 32 34 62 40 87 8 114 76 149 3 36 36 36 36 116 72 144 5 20 40 40 56 16 90 36 116 67 116 67 146 67 116 67 146 67 116 67 116 67 116 67 116 67 144 67 116 67 116 67 116 67 116 67 116 67 116 67 116 67 116 67 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116	w		30	**	09	ייי ו	65	0	112	50	139	
2 12 37 46 62 46 68 24 116 72 144 4 36 36 46 56 64 56 116 72 144 5 20 41 26 46 56 46 56 66 117 32 117 32 7 28 42 12 66 16 92 24 119 56 16 8 32 46 4 69 16 70 118 116 70 116 70 116 70 116 70 116 70 116 70 116 66 66 126 24 116 70 116 70 116 70 116 70 116 70 116 70 116 66 66 66 126 126 126 126 126 126 126 126 126 126	10	24	36	**	19	111	86	•	113	20	140	. 22
3 36 44 63 36 69 24 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 60 116 <t< td=""><td>12</td><td>15</td><td>37</td><td>46</td><td>62</td><td>40</td><td>18</td><td>•</td><td>111</td><td>76</td><td>143</td><td>•</td></t<>	12	15	37	46	62	40	18	•	111	76	143	•
4 36 36 36 36 36 36 36 36 36 36 31 117 32 60 118 117 32 117 32 117 32 117 32 118 116 60 116 59 32 119 116 60 116 119 116 119 116 119 116 119 116 119 116 119 116 116 116 119 116 119 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116 116	13	38	36	44	6.3	36	88	24	115	72	144	•
5 20 40 40 40 40 41 26 44 50 32 117 7 28 42 12 67 26 16 92 24 118 9 52 44 4 69 16 92 26 120 1 22 46 69 16 70 12 26 120 1 32 46 69 16 52 121 2 46 46 70 12 56 122 2 46 46 72 62 123 124 4 46 73 40 60 99 72 124 4 46 73 73 40 99 72 128 4 46 74 74 100 76 129 5 40 52 100 77 44 102 32	-	36	36	32	49	56	68	36	116	99		
6 20 41 26 16 92 24 119 7 28 42 12 67 26 92 24 119 8 32 44 4 69 16 53 26 120 9 12 69 16 54 28 161 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 120 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 121 </td <td>15</td> <td>20</td> <td>94</td> <td>74</td> <td>65</td> <td>**</td> <td>05</td> <td>32</td> <td>117</td> <td>32</td> <td></td> <td></td>	15	20	94	74	65	**	05	32	117	32		
7 28 42 12 67 26 92 24 119 8 32 43 16 68 16 93 20 120 9 52 44 4 69 16 54 26 121 1 32 46 16 70 12 54 26 121 2 46 16 71 40 65 28 123 123 2 46 46 72 65 97 40 123 4 46 32 73 40 60 120 123 5 40 46 74 74 60 100 76 128 6 56 51 66 51 75 40 101 52 120 7 32 100 76 40 102 26 123 8 44 55 42	91		;	26	99	16	15	0.4	118	116		
8 32 43 16 68 16 53 20 121 54 28 181 181 181 181 181 182 182 182 182 182 182 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 183 184 183 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 184 183 <	17		42	12	49	26	92	24	611	800		
9 52 44 4 69 12 95 28 121 1 32 46 16 71 40 95 28 123 2 28 47 36 72 62 32 123 3 24 46 72 62 98 32 124 4 46 32 73 40 60 99 72 124 4 46 32 73 40 60 99 72 124 5 40 52 74 74 60 99 72 128 6 56 50 75 56 100 76 129 7 32 100 77 44 102 32 130 8 54 14 79 36 104 8 133 9 44 55 42 80 56 104	18		E.4	16	68	16	63	20	120	100		31
0 12 45 6 70 12 95 28 123 2 28 47 36 72 62 97 40 123 3 24 46 32 73 40 98 32 123 4 8 45 44 74 60 99 72 124 5 40 50 75 56 100 76 129 6 56 50 100 76 101 57 128 7 32 56 100 76 101 52 130 7 32 100 77 40 101 52 130 7 32 100 77 44 102 32 131 8 43 54 14 79 36 104 8 134 1 72 36 42 10 10 10	5.		44	•	69	12	45	28	121	6.6		
1 32 46 16 71 40 96 32 123 2 4 46 32 73 40 98 32 124 4 8 45 44 74 60 99 72 124 6 50 20 75 60 99 72 128 6 56 40 75 56 100 76 129 7 32 51 62 76 101 52 130 8 44 52 100 77 44 102 32 131 9 43 54 14 79 36 104 8 133 9 44 55 42 106 12 133 9 44 55 42 104 8 133 1 72 36 42 104 8 133 1 72 36 42 106 12 135 1 72 36 42 106 12 135 1 72 36 70 83 24 110 24 137		12	4	Ą	02	12	35	28	122	96		
2 28 47 36 72 62 97 40 124 4 8 46 32 73 46 98 32 127 4 8 45 44 74 60 99 72 128 5 50 20 75 56 100 76 129 7 32 51 62 76 40 101 52 130 8 52 100 77 44 102 32 131 9 44 53 100 78 42 103 26 132 9 44 55 42 14 102 32 131 9 44 55 42 104 8 103 26 132 1 72 56 70 81 32 104 8 135 2 64 57 36 70		32	+ ·	16	711	46	95	. 32	123	•		1
24 46 32 73 46 99 32 127 4 8 45 44 74 60 99 72 128 6 56 20 75 60 99 72 128 7 32 20 75 40 76 101 52 130 7 32 100 77 44 102 32 131 8 43 54 14 79 38 104 8 133 9 44 55 42 80 56 106 12 133 1 72 36 16 16 135 1 72 36 10 60 10 135 2 64 57 36 70 83 24 110 24 137		28	47	36	72	(2)	97	0.	124	•		
4 8 45 44 74 £0 99 72 128 6 £6 £0 20 75 £6 100 76 129 7 32 £2 76 40 101 52 130 6 £6 52 100 77 44 102 32 131 7 44 53 100 78 42 103 26 133 9 44 55 42 80 50 104 8 133 1 72 56 70 81 52 107 16 135 2 64 57 36 70 83 24 110 24 137		24	46	(N)	73		86	32	127	24		
€ 40 50 20 75 56 100 76 129 7 32 51 £2 76 40 101 52 130 7 32 52 100 77 44 102 32 131 9 43 53 100 78 42 103 26 133 0 44 55 42 80 60 106 12 133 1 72 56 70 81 52 107 16 135 2 64 57 36 70 83 24 110 24 137		80	54	44	74	60	66	72	128	26		
6 56 56 51 62 76 40 101 52 130 7 32 100 77 44 102 32 131 6 44 53 100 78 42 103 26 132 9 44 55 14 79 36 104 8 133 1 72 56 70 81 32 107 16 135 2 64 57 36 70 83 24 110 24 137		40		20	75	56	100	26	129	48		
7 32 52 100 77 44 102 32 131 6 44 53 100 78 42 103 26 132 9 43 54 14 79 36 104 8 133 0 44 55 42 80 50 106 12 134 1 72 56 70 81 22 107 16 135 2 52 56 70 83 24 110 24 137				(4)	92	94	101	52	130	20		
6 44 53 100 78 42 103 2e 132 9 43 54 14 79 3e 104 8 133 10 44 55 42 80 50 106 12 134 1 72 56 70 81 3c 2c 107 16 135 2 64 57 3e 82 2c 100 24 137 3 5c 70 83 2c 110 2c 137		32			11	4.4	102	32	131	70		
9 43 54 14 79 38 104 8 133 0 44 55 42 80 56 106 12 134 1 72 56 76 81 32 107 16 135 2 64 57 36 82 26 108 4 126 3 52 56 70 83 24 110 24 127		**		100	7.8	14	103	26	132	116		
0 44 55 42 80 56 106 12 124 1 72 56 76 81 32 107 16 135 2 64 57 36 82 26 108 4 136 3 52 58 70 83 24 110 24 137		43		=	29	36	104	80	133	79		,
1 72 56 70 81 32 107 16 135 2 64 57 36 82 20 108 4 126 3 52 58 70 83 24 110 24 137		:	55	42	90	99	106	12	134	36		
2 58 70 83 24 110 24 127		72	56	20	18	ייי	101	91	135	91		
2 58 70 83 24 110 24 137	3.5	64	57	36	82	26	108	4	136	20		
	(7)	52	58	7.0	83	24	110	24	137	•		

STAGE 1. WING 6. TF-HI011. SOL GEL. CRCSSLINK DENSITY

This sample size summary is applicable to figures 56 and 57.

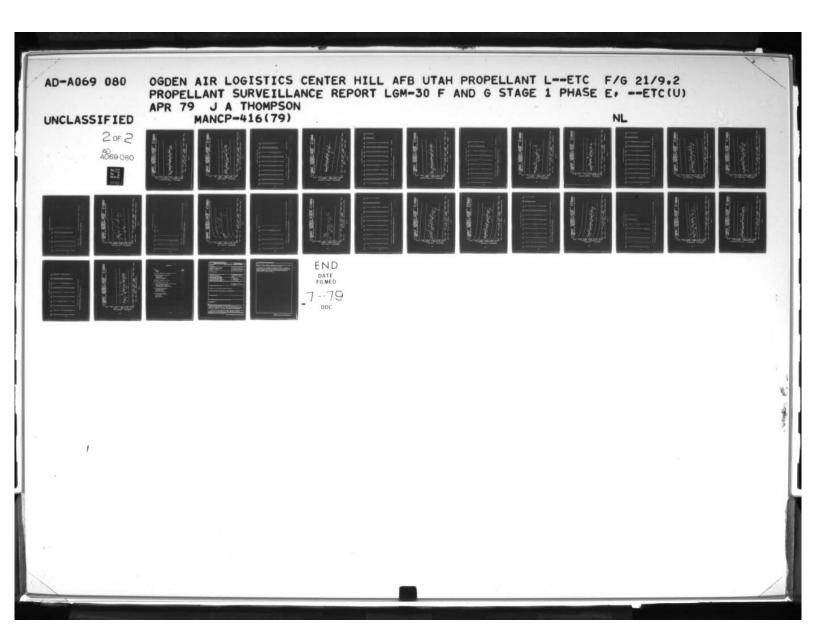
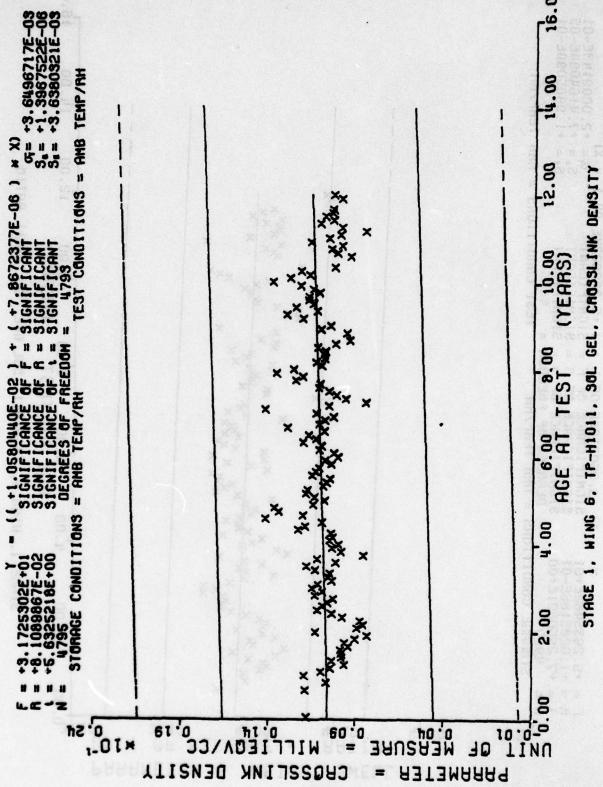
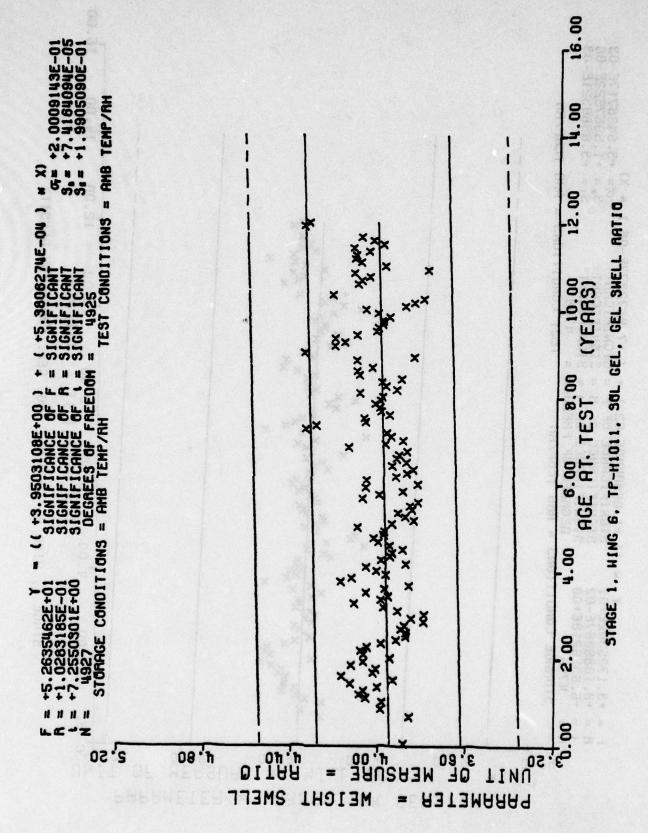


Figure 56





*** SAMFLE SIZE SUMMARY ***

SARB	v	90	63	18	13	30	12	12	27	75	9	12	•	1.6	63	E A	v	E	m						
166	129	130	131	132	133	134	135	136	137	138	139	140	151	142	143	144	146	146	991						
SAR	36	16	11	v	r)	m	m	5	9	33	30	17	22	104	**	51	34	104	31	63	7.6	42	us.	v	5
(NGE (NGE)	100	101	102	103	104	105	1 06	107	108	109	110	===	112	113	114	115	116	117	116	119	120	121	122	125	128
SAN	43	w)	E. 4	7.2	1.3	4 6	4.2	23	25	91	91	54	רי) יין	63	43	4.5	E) (1)	26	91	1:	r)	44	69	63	38
AGE (POS)	75	26	77	78	79	90	18	82	83	84	69.53	96	87	86	68	06	9.1	92	63	46	50.00	96	97	96	(A
SAR	13	9	95	72	42	26	62	59	13	23	20	27	63	56	65	22	01	3.6	13	(C)	:	26	21	99	13
AGE (POS)	36	91	52	63	99	56	96	57	56	56	99	19	62	63	99	99	99	67	99	59	22	11	7.2	73	7.4
SAKP	51	*9	22	58	34	69	31	5	67	96			26		26						01	25	36	37	64
AGE PCS 1	24	25	26	27	28	53	36	31	35	F)	47	3.6	36	37	36	38	04	+	4.2	4.2	44	46	47	48	45

CCASTANT STRAIN TP-H 1011 BING 6 STAGE 1

This sample size summary is applicable to figure 58.

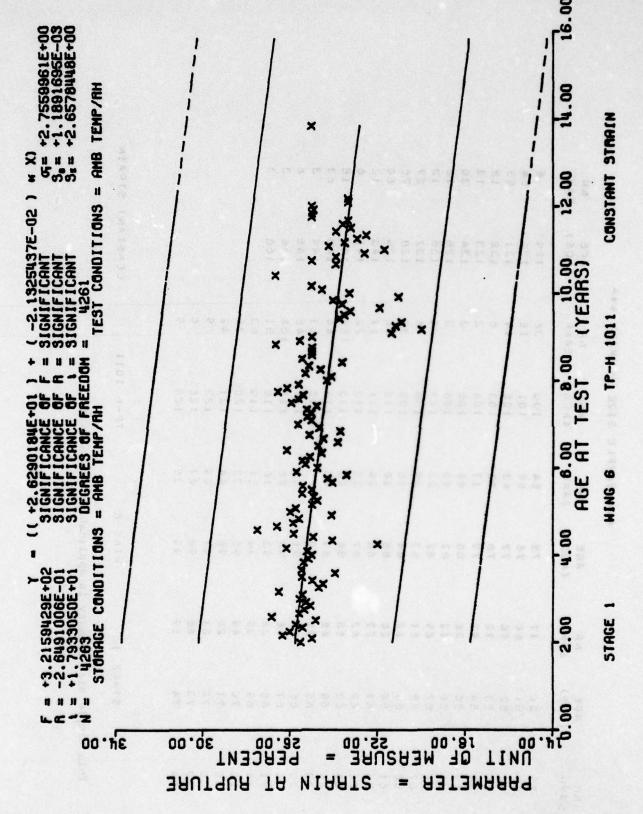


Figure 58

** SAMFLE SIZE SUMMARY ***

					37,440	3712	- LECEDO	TO PECONE			
AGE MCS)	SARP	AGE (POS)	0 A A A	16E (10S)	SAVE	AGE (PCS)	SARR	AGE (PCS)	SAR	AGE (MOS)	# 4 W
•	99	58	52	£0	4.0	79	46	104	w	134	16
•	108	30	ęę	55	73	90	57	901	w	136	16
w	126	31	53	56	99	18	8	101	01	136	30
1	1117	32	20	57	63	82	66	110	21	137	==
•	1117	33	53	5.0	69	83	17	111	12	138	(7)
•	129	34	47	25	73	40	7	112	21	139	45
10	=	36	•	9	£.	85	20	113	40	140	12
1.1	126	36	15	19	60	98	46	*::	13	=	2
12	63	37	36	62	99	67	30	116	•	**1	21
13	106	36	99	63	\$ 02	88	20	911	33		
	110	36	94	• 9	:	6.8	33	117	E E		
50	135	94	36	69	99	05	64	118	w		4
16	126	11	46	99	63	∞ 15	25	611 ×	σ.		
17	136	42	93	67	4.6	92	04	120	× 27		
18	108	43	31	69	67	66	32	123	12		
51	52	:	")	69	113	*6	25	124	12		
20	27	45	W) P)	70	137	65	56	126	27		
21	20	94	99	71	46	96	× 17	126	1.8		
17	33	14	54	72	36	25	73	127	33		
23	92	48	101	73	40	96	56	128	33		
24	57	54	20	7.4	201	65	56	129	24		
25	36	9	13	75	73	001	46	130	36		
26	99	51	112	9/	60	101	w	131	80 FO		
27	42	52	112	77	72	102	12	132	91		
28	36	60	14	7.8	72	103	16	133	16		

This sample size summary is applicable to figure 59.

HARDNESS

SPORE A. 10 SECCIC

TF-H 1011

STAGE I NING 6

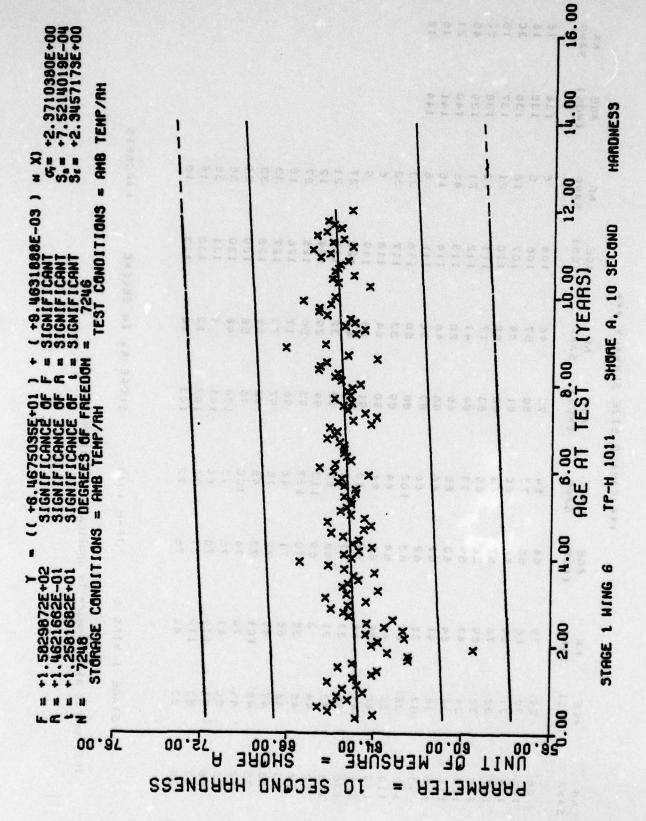


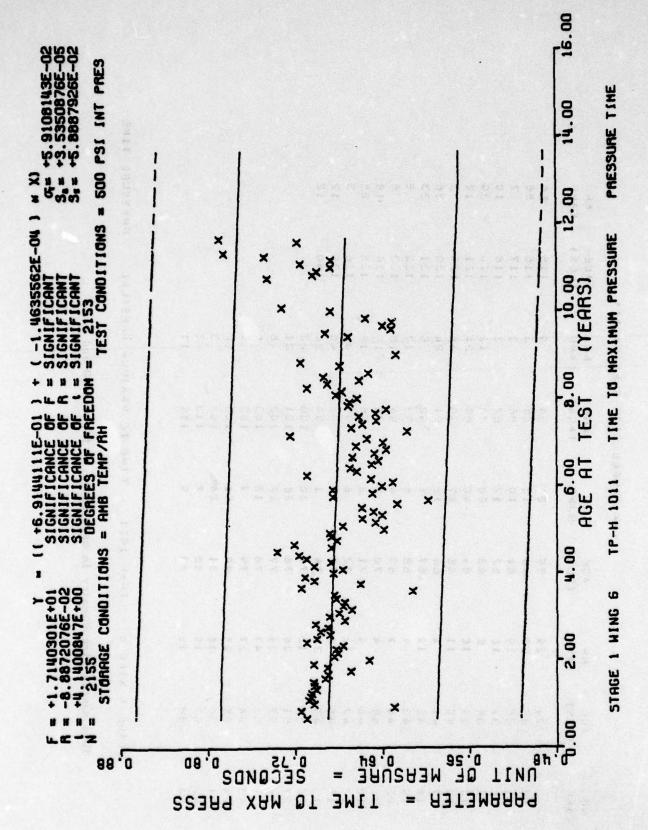
Figure 59

** SAMFLE SIZE SUNNARY ***

SAME	56	W)	1	01	39	12	E)	36	33	6 7	w	10	26	m	12	12									
(PCS) S	115	116	117	118	150	121	125	130	131	132	133	134	9:7	136	139	140									
SAKE	v	m	r,	ניז	21	24	36	24	υ,	17		51	# 91 *	36	0.7	26	23	21	æ	¥	y.	ψ	ניז	ניז	
(808)	8.4	er er	96	67	43	683	30	91	55	€5	84	95	95	97	98	6.5	100	101×	102	103	105	106	108	113	114
SAPE	24	13	01	1.7	50	4 6	27	16	w	ų,	4		(V	ý	W	-	36	26	22	13	1	6.1	24	,	U
(80%)	5.5	00	61	62	63	40	O. (A	óó	67	68	5.9	70	17 €	72	73	7.4	7.5	76	77	7.8	79	90	19	92	2 4
SANE	50	60	35	10	w	31	=	•	12	•	1	4	138	13	4	30	13	3¢	35	47	37	47	16	16	*-
(NCS)						3.5																			
SANE	۲)	91		v	152	13	10	17	an 1	51	22	93	- 13	13	ş; T	13	25	27	36	93	43	54	16	42	6.4
NCS)	w.	2	=	12	==	14	===	-	11	1.8	51	20	2.1	19	23	54	25	56	27	2.6	23	36	31	(2)	

TP-H 1011 TIME TC MAXIMUM PRESSURE PRESSURE TIME STAGE I NING 6

ry is applicable to lighter to the same of This sample size summary is applicable to figures 60 and 61.



88

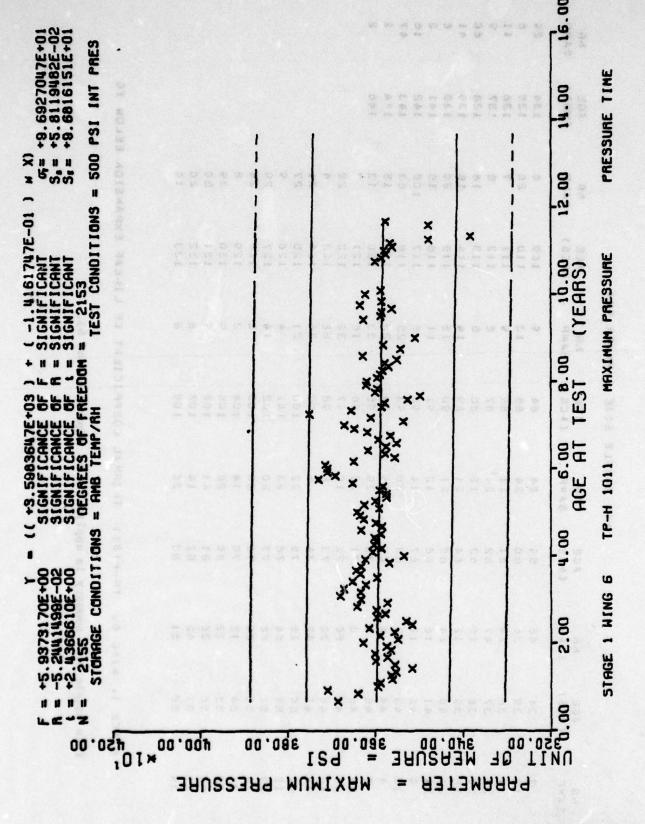


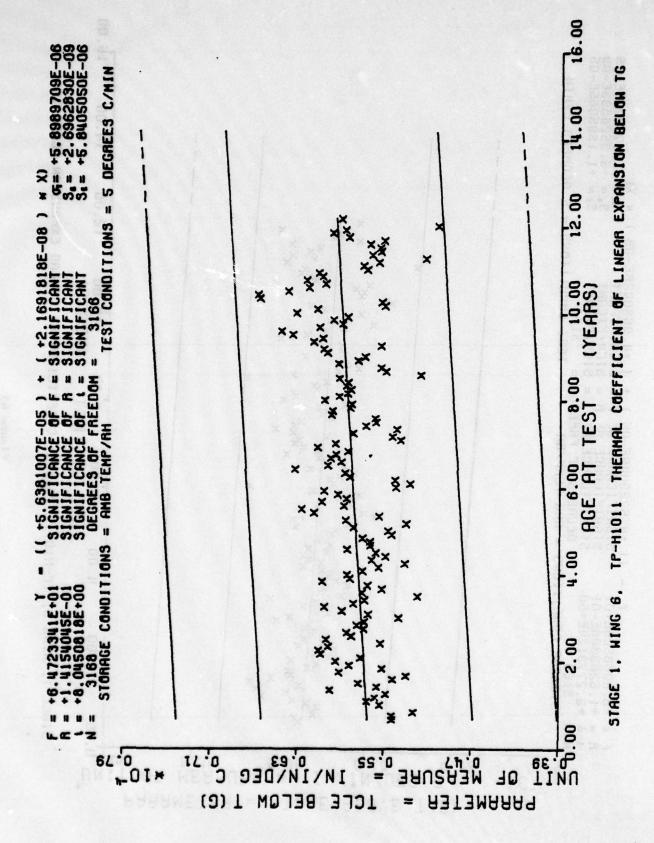
Figure 61

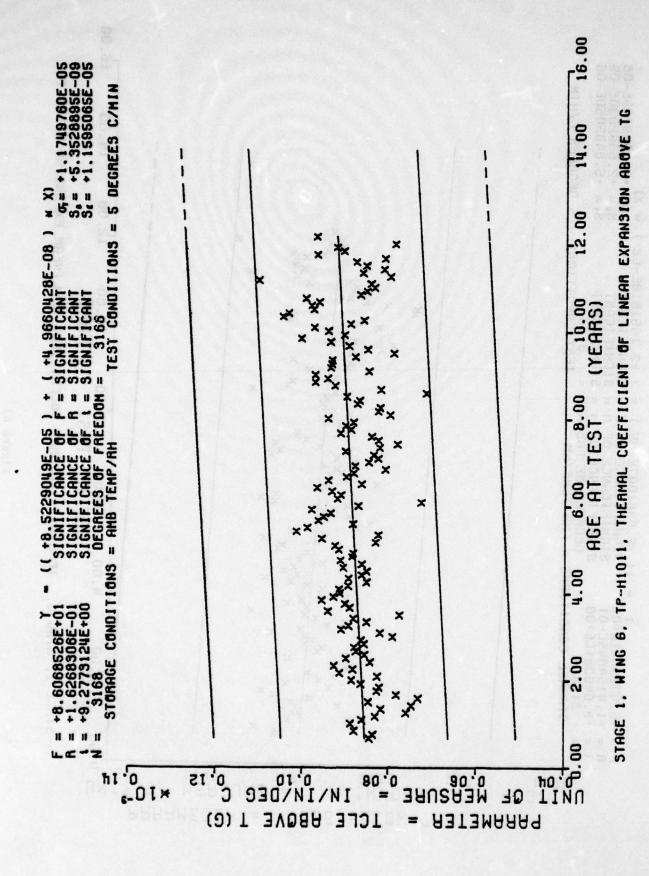
*** SAMFLE SIZE SLMMARY ***

N A A A	25	•	=	•	. 60	=	•		91		••	8									•	*			
CMOS)	134	135	136	137	138	139	140	==	142	143	**1	146										•			
SAND	w	20	1	vo	91	92	20	15	106	63	10	13	7	28	•	21	27	•	53	24	•	39	20	20	•
(PCS)	601	110	===	112	113	*::	115	116	117	911	119	120	121	122	123	124	125	126	127	128	129	130	131	132	
SARP	•	13	us.	•	w	=	91	=	w	25	23	33	91	32	99	36	21	•	*1	w	m	v	s	æ	•
() () () () () ()	64	82	96	97	88	69	05	115	55	63	96	96	95	25	86	65	100	101	102	103	104	105	106	107	00.
SAVE	24	24	113	21	12	-: (V	12	12	*-	26	53	39	20	91		10	(3	23	20	35	14	26	1.1	41	00
(104)	55	99	19	62	63	64	6.5	99	67	68	69	20	112	72	73	7.4	7.5	92	77	7.8	4	80	18	82	
1 4 4 8 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	- T	36	5.4	47	91	12	54	31	12	12		5	r)	2	32	42	## (V	64	99	38	97	r) m	36	42	
(NOS)	34	35	36	37	36	39	04	-	42	43	44	46	94	4.7	48	45			52	53	6.4	99	56	57	
SARP	f	01	1	22	52	15	21	24	0	33	•	0	26	24	12	81	45	91	27	24	38	42	48	4.0	7.
AGE (MCS)	w	•	10	12	13	:	==	91	1.7	1.8	51	20	21	22	23	54	25	26	27	26	25	30	31	(3.6)	,

STAGE 1, WING &. TP-FI011 THERMAL COEFFICIENT OF LINEAF EXPANSION EELOW TG

This sample size summary is applicable to figures 62 and 63.





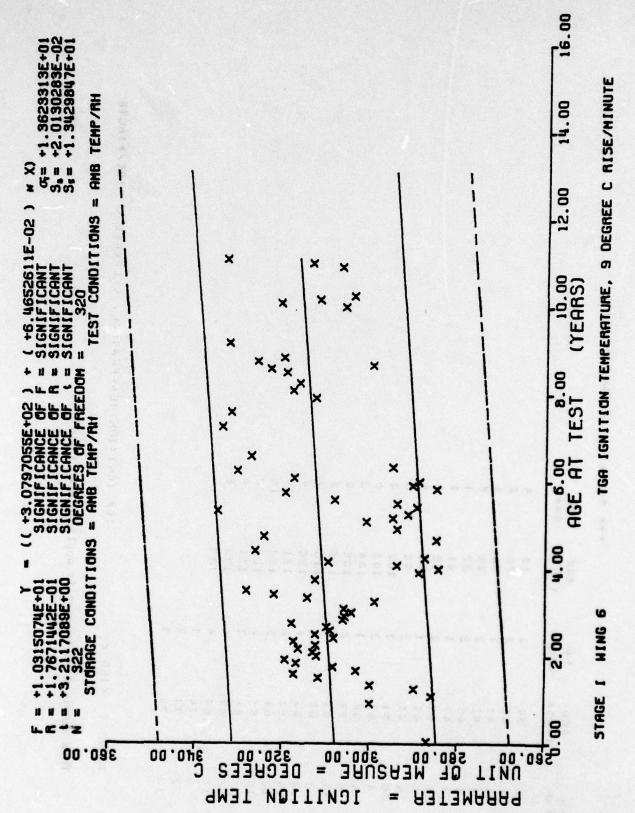
- 92 -

*** SAMFLE SIZE SUNMARY ***

2	3 G E	1 4	מיט אַ	N N N	
SANE	(604)	TARS	(100)	1240	
ניז	36	1")	73	•	
S 133	240	m	75	(V	
-	4.1	۳)	92	1	
	42	17)	52	•	
1	4	"	87	-	
7	47	-	15	1	
(V	94	w	35		
4	54	-	15	¥	
4	36	"	56	6	
20	21	ניו	102	1 × 1 × ×	
4	53	m)	103	•	
4	56	-	104	••	
v	57	۳)	105	N	
14	53	-	106		
2	19	1 288c 3	110	"	
4	62	1 36 70	120	•	
14	63	(1)	121	21	
12	64	ניז	122	91	
10	W (2)		123	~:	
2	99	-	131	•	
y	67	4	132	¥	
16	59	4	133	.,	
5	22	-			
22	11	(V			
1.3	10	•			

TEA IGNITION TEMPERATURE, 9 CECREE C RISE/MINUTE STAGE I WING &

This sample size summary is applicable to figure 64



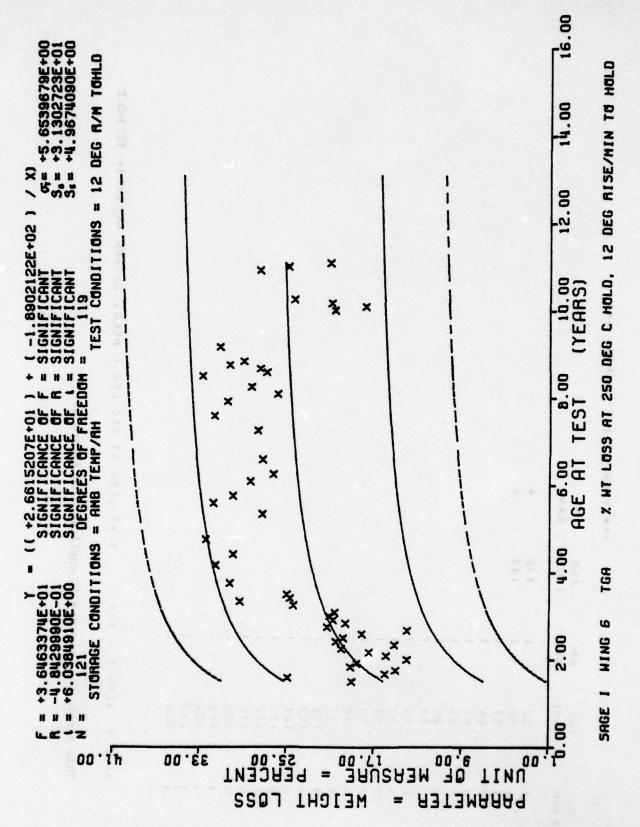
2 60 1 132 A 100 67 1 133 2 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	AGE	2 2	AGE	Q 2	AGE	7 V V	1750523	
3 66 10 67 10 67 11 133 8 2 64 11 67 12 65 13 76 14 104 1 106 1 106 1 110 1 110 1 110 1 110 1 110 1 110 1 110 1 111 1 1 1 1	(5)4	SANE	(504)	SAPE	(NOS)	SAFE	00 0	15.00
10 64 11 133 2 2 64 1 1 133 2 2 64 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13	*	96	7	132	•		
10 64 11 10 65 11 11 10 65 11 11 10 65 11 11 10 65 11 11 10 65 11 11 10 65 11 11 11 11 11 11 11 11 11 11 11 11 11	15		53	-	133	w		
2 64 11 2 65 11 3 75 51 1 87 75 6 97 8 6 1 106 1 116 1 120 1 123 1 131 2 133	20		57	7				
10 67 73 75 75 75 75 75 75 75 75 75 75 75 75 75	21	2	64					
2	22	10	19	•				
2 73 73 1 75 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	53	2	59	-				
7 7 7 6 1 1 1 67 7 7 6 7 7 6 7 7 6 7 7 6 7 7 6 7 7 7 6 7 7 7 7 7 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	24	N.	73	7				
6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	25	r)	76					
6 6 6 7 7 8 8 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	26	7	54	×				
6 97 65 11 102 11 106 11 120 6 11 120 6 11 120 6 11 11 120 6 11 123 1 131 2	27	-	67	. ×				
6 95 1 1 102 1 3 103 2 4 104 1 1 106 1 1 120 2 1 123 2 1 123 2	28	(2)	15	- × ×				
6 97 6 1 102 1 1 103 2 1 104 1 1 110 1 1 120 2 1 123 2 1 123 2 1 133 2	15.	四.四	95	×				
6 6 106 1 1 1 1 1 2 2 2 2 2 2 3 3 3 3 3 3 3 3 3	30	ę	15	tu Z				
1 102 1 2 103 2 2 105 1 6 106 1 1 120 2 1 122 6 1 123 1 1 133 2	31	153	55	-				
3 103 2 2 104 1 1 106 1 1 120 2 1 1 1 1 1 2 1 1 2 1 1 1 1 2 1 1 2 1 1 1 1 2 1 1 1 2 1 1 1 2 1 1 1 2 1 1 2 1 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 1 1 1 2 1 1 2 1 1 1 1 1 1 1 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3.5	-	102	-				
6 104 1 1 106 1 1 120 2 1 123 2 1 133 2	63	E)	103	(V				
6 106 1 1 106 1 1 120 2 1 123 6 1 133 2	34	4	104	3%				
6 106 1 1 120 2 1 122 6 1 123 1 1 133 2	4,6	~	165	-				
110 110 1 120 2 1 1 121 5 1 1 1 1 1 2 3 1 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 3 1 2 2 1 1 1 1	41	ę	106	-				
1 120 2 1 121 5 1 1 123 1 1 1 133 2	37	10.	110	7				
1 121 5 1 122 6 1 123 1	38	-	120	(V				
1 122 E 1 123 1 1 131 2	40	-	121	K)				
1 123	11	-	122	¥ /				
1 131	43	•		-/				
	9.0	-		N				

X WI LCSS AT 25C DEG C HCLD. 12 DEG RISEZWIN TC FOLD 1GA SAGE I WING 6

This sample size summary is applicable to figure 65

DISTRICTOR CARD OF SALE

JEST CONDITIONS - IS DEC BYR JOHN

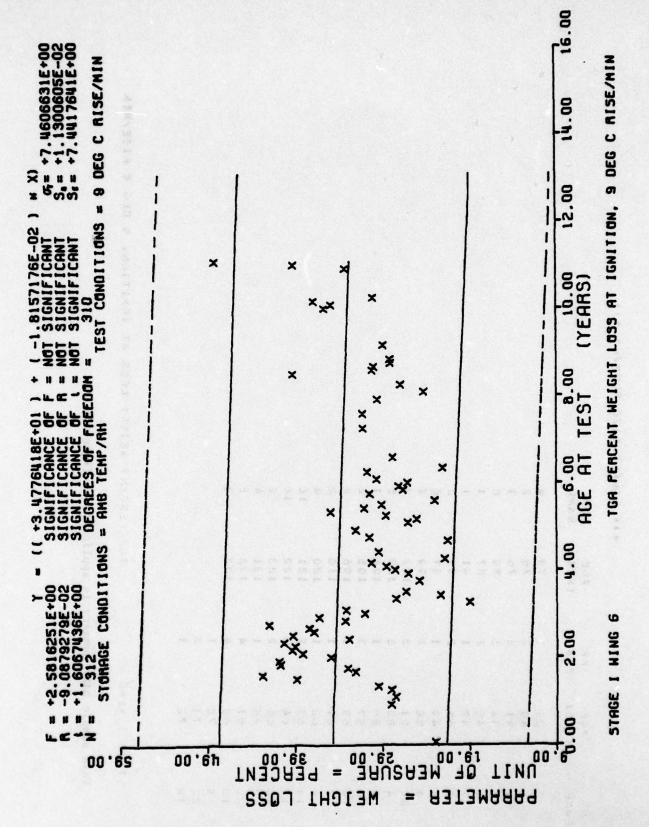


*** SANFLE SIZE SUMMARY ***

7 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4

TGA FERCENT WEIGHT LCSS AT IGNITION. 9 DEG C FISE/MIN STAGE I WING 6

This sample size summary is applicable to figure 66



*** SAMFLE SIZE SLMMARY ***

STAGE I WING 6. TF-F 1011. CTA, ENCCTHERM 1. 12 DEGREE CENTIGRADE FISE/WIN

This sample size summary is applicable to figures 67 and 68.

- 100 -

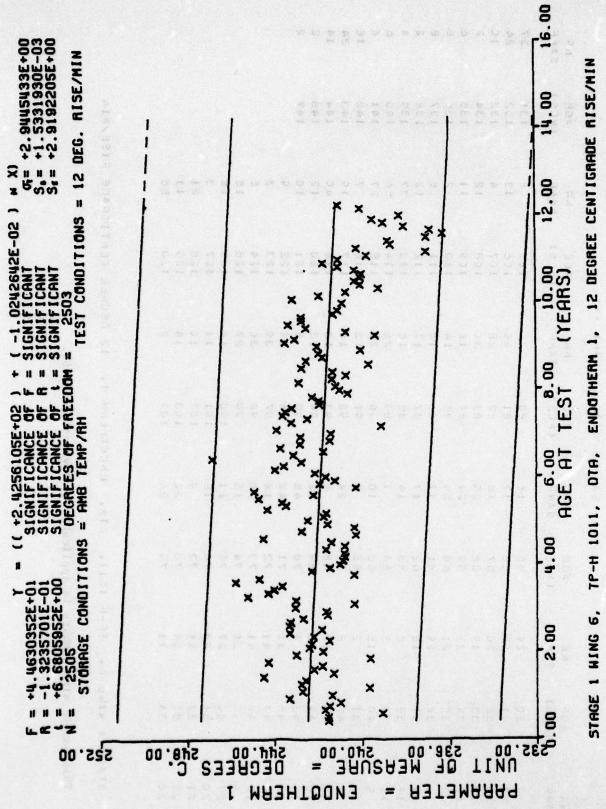
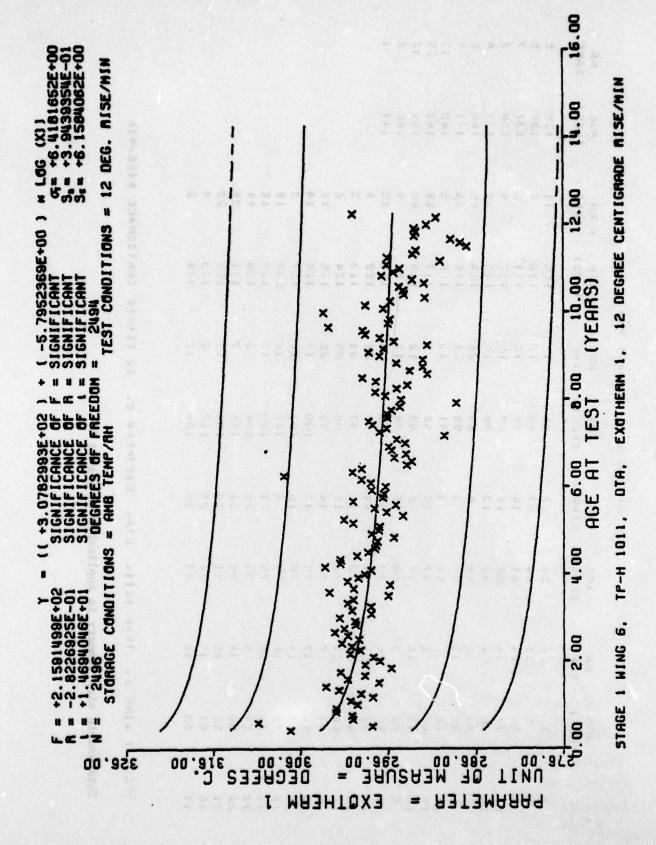


Figure 67

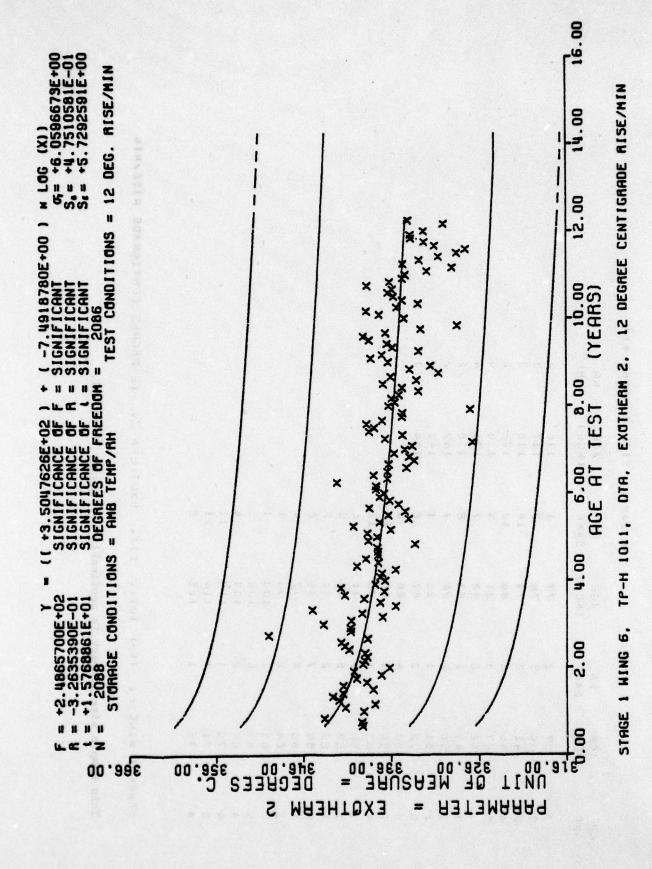


*** SAMPLE SIZE SUMMARY #**

4 4		w	Q	1	"	•	9	w)	13	53	12	~	-				-									
AGE	(873)	136	136	137	138	139	140	141	142	143	144	146	147													
A P P P P P P P P P P P P P P P P P P P	1245	7	(V	w	o,	36	(D)	24	S)	16	40	•	10	v	m ×	æ	15	=	r)	16	<u>.</u>	*	W) ED	22	au	•
AGE	(100)	109	110	==	112	113	4:-	115	116	× 117	118	120	151	122	183	154	125 × 125	126	127	128	169	130	131	132	133	134
N. P.	FAR	91	12	12	15	16	28	31	13	5	12	12	4	36	31	52	25	1.4	10	10		(V	7	13	w	31
A GE	-	84	85	86	87	a: a:	68	× 05	15	55	63	45	96	95	97	96	65	100	101	102	103	104	106	901	107	105
N. C.	SANT	22	27	14	16	13	9	(JA	5	2.5	w	51	38	4.1	× 16	16	14	1.7	16	5	12	26	13	52	26	36
AGE	(804)	5.6	6.0	61	62	6.0	64	65	99	57	68	69	7.0	11	7.2	73	74	7.5	76	77	7.8	7.9	80	16	82	4.7
7 Y	444	26		5.4		4	"	13	(V	w	10	(*) 	9	σ	36	× 11 × ×	3.0	17	4.	1e	W. (2)	v	16	91	17	7
AGE	(SON)	34					3.5			42	4 60	44	4 5	4	14	84	D 4	99	£1	53	63	64	999	56	57	
2	SAME	r	u)	m	1.1	10	U	U)	51	14		4			E					12						
AGE	(50)	Ą	5	10	12	22	14	15	16	17	1.8	15	20	12	22	2	24	25	26	27	28	50	30	31	3.5	2.3

STAGE I WING &. TE-H 1011, CTA, EXCTHEFN 2, 12 CEGREE CENTIGRADE FISE/WIN

This sample size summary is applicable to figure 69.

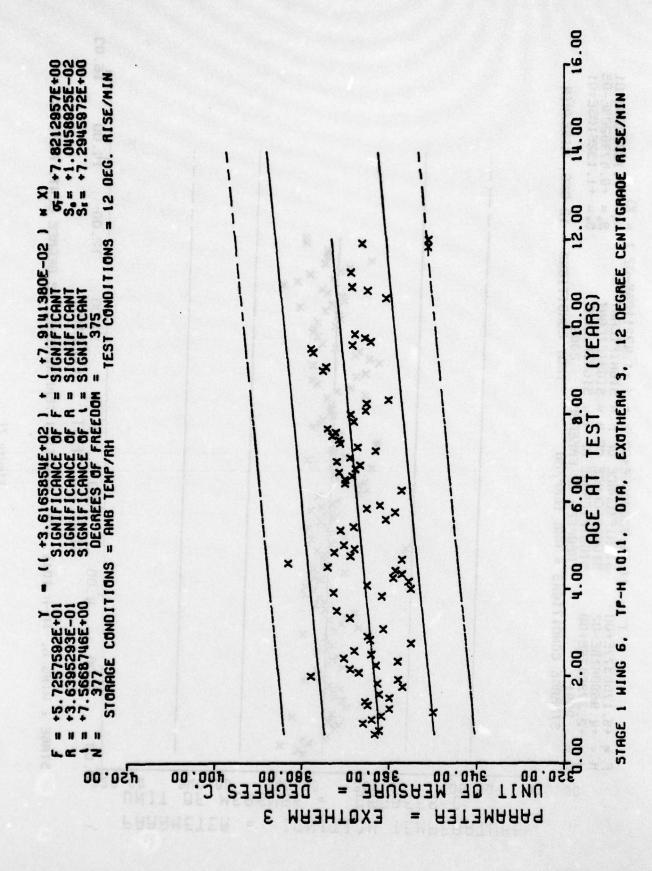


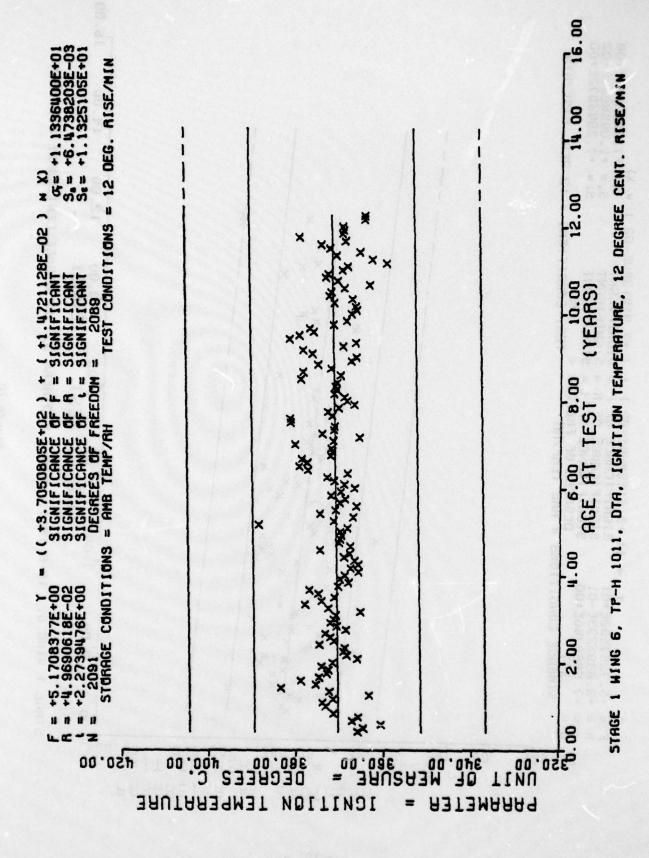
1	
* * *	
-	
>	
1	
AA	
-	
-	
2	
SLR	
-	
,	
Description of the last	
U)	
-	
2E	
-	
U	
7.7	
L	
_	
AMFL	
-	
-	
-	
- Q	
U	
U)	
-	
*	

AGE NCS 1	SANE	(POS)	SAR	AGE (ACS)	SAN	AGE (PCS)	SAR	
w	n	37	m	7.7	-	116	N	
u	1	94	(y	78		117	וה	
11	F)	42	ניח	54	16	118	ניז	
12	•	40	30	80	12	126	(N	
	u)	47		31	O.	130	S.	
14	r)	4.8	Ü	82	7	131	4	
15	-	54	(V	83	æ	136	(4	
16	e	56	2	45	2	142	Ci	
17	"()	61	-	9.6	-	143	4	
18	v	52	m	97	8	144	XX IXX	
51	¥	E)	4	88	80			
12	W	54	×	68	16			Today of
22	4	55	XX Iso	90	12			
ניו		56		31	•			
24	1	57	u,	55	W			
25	1	5.8	(1)	9.6	(V			
55	(V	55	7	96	v			
27	4	99	4	3.7	4			
20	ניו	64	(V	55	-			
52	4)	Ġ.S.	(V	100	-			
30	v	67	9	108	ניו			
31	4	59	(V	501	4			
63	4	7.0	-	113				
34	(I)	12	1	114	12			
4		76			u			

STAGE I WING &. TF-H 1011, CTA, EXGTHERN 3, 12 DEGREE CENTIGRADE RISE/MIN

This sample size summary is applicable to figures 70 and 71.





- 106 -

*** SAMFLE SIZE SLMWARY ***

\$\text{SAMP}\$ (MOS) SAMP (MOS) SA	SE	4	AGE	A A	AGE	Œ	A GE	æ	AGE	4
41 6 75 57 100 22 15 15 15 15 15 15 15 15 15 15 15 15 15	5	SAMP	(NOS)	SAND	(NOS)	SANE	(NCS)	SAKE	(FCS)	SAPE
1	5	n	7	v	75	57	100		129	39
16 47 3 77 21 102 16 12 63 1 78 8 103 3 16 54 26 6 15 106 3 3 56 17 82 21 107 3 3 56 17 82 21 109 3 3 56 17 82 21 109 3 24 81 17 26 109 3 25 17 82 21 109 3 27 60 36 6 111 112 46 60 36 6 113 16 47 60 36 6 114 116 22 47 60 36 10 116 22 14 40 64 26 90 10 116 20 43 65 16 12 11 12 14 43 70 2 9	9	•	42	<u> </u>	16	36	101	v	130	48
12 52 1 78 8 103 3 18 54 26 79 35 105 3 3 55 24 81 28 106 3 3 56 17 82 21 106 3 3 56 17 82 21 106 3 24 60 17 83 11 11 12 27 61 16 85 5 111 11 12 46 62 40 86 6 113 14 40 47 99 10 12 114 51 14 41 41 48 60 36 36 6 6 114 51 14 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41 41		10	47	m	77	1.2	102	31	131	63
12 63 6 79 39 105 3 3 55 24 81 28 107 3 3 56 17 82 21 109 3 3 56 17 82 21 109 3 24 83 15 110 3 111 112 25 84 5 111 12 14 27 61 16 87 6 113 16 46 62 40 86 6 113 16 47 40 88 12 114 47 46 63 36 6 116 22 47 60 16 12 116 22 47 65 16 6 120 77 43 66 3 6 120 22 43 66 6 16 122 18 43 70 3 95 14 122 14 </td <td></td> <td>12</td> <td>52</td> <td>1</td> <td>78</td> <td>60</td> <td>103</td> <td>E)</td> <td>132</td> <td>24</td>		12	52	1	78	60	103	E)	132	24
18 54 26 80 15 107 3 3 55 24 81 28 108 3 3 56 17 82 21 109 3 3 56 17 24 83 16 110 3 24 60 33 85 9 111 12 27 61 16 86 6 113 16 46 62 40 86 6 113 16 46 62 40 88 12 114 51 47 62 40 88 12 116 22 48 64 6 10 116 22 117 21 49 66 10 22 117 20 23 14 120 77 49 66 6 6 6 12 14 12 14 43 66 6 6 16 12 14 12 14		12	63	y	19	38	105	נית	133	11
3 55 24 81 28 108 3 3 56 17 62 21 109 3 3 56 17 24 83 16 110 3 24 60 35 85 9 111 12 14 27 61 16 86 6 113 14 47 46 62 33 85 9 111 115 47 46 62 40 88 12 115 47 47 99 10 22 115 47 48 66 6 9 6 120 77 49 6 6 12 11 118 22 49 6 6 12 12 12 49 6 6 12 12 12 49 6 6 12 12 12 49 72 24 96 16 12 6		1.6	54	3.6	90	5	107	E)	134	91
3 56 17 82 21 109 3 3 56 25 84 5 111 12 110 12 14		n	(S)	24	91	28	108	E .	135	16
3 56 35 64 5 111 12 14 12 14 6 15 15 15 15 15 15 15 15 15 15 15 15 15		3	26	17	82	2.1	501	ניז	136	5
3 56 33 85 9 111 12 14 12 14 6 60 33 85 9 6 113 114 12 14 6 60 35 86 6 113 114 51 14 6 62 40 88 12 115 115 14 51 14 6 63 36 89 10 116 22 117 21 118 23 119 27 29 67 3 99 33 128 9 9	_	~	57	24	83	1.6	110	m	137	5
24 60 35 95 9 112 14 27 61 15 62 40 86 6 113 16 46 62 40 86 12 114 51 18 63 36 89 10 116 22 42 64 27 91 11 118 23 43 66 3 92 23 119 23 43 66 3 92 23 119 27 43 70 3 93 6 120 77 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 22 127 22 15 74 47 99 33 128 9 12 22 99 33 128 9		e	56	5 17	84	5	111	12	138	9
24 60 35 86 6 113 16 46 62 40 88 12 114 51 18 63 36 89 10 116 22 42 64 20 90 22 817 21 31 65 10 91 11 118 23 43 66 3 92 23 119 27 43 66 3 92 23 119 27 43 70 3 95 14 122 18 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 74 47 99 33 128 9		0	5:3	33	85	5	112	14	139	:
27 61 15 67 3 114 51 46 62 40 88 12 115 47 18 63 36 89 10 116 22 42 64 20 90 22 117 21 31 65 10 91 11 118 23 43 66 3 92 23 119 27 43 70 3 95 14 122 18 43 70 3 95 14 122 18 43 70 3 95 14 122 18 43 72 24 96 16 123 9 14 72 24 97 22 127 22 15 74 47 99 33 128 9			9	90	98	y	113	16	140	21
46 62 40 88 12 115 47 18 63 36 89 10 116 22 42 64 26 90 22 117 21 31 65 16 91 11 118 23 43 66 3 92 23 119 27 43 67 3 94 6 120 77 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 74 47 99 33 128 9			19	91	67	Б.	114	21	141	24
18 63 36 89 10 116 22 42 64 20 90 22 117 21 31 65 10 91 11 118 23 43 66 3 92 23 119 27 29 67 3 94 6 120 77 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 73 25 98 32 127 22 15 74 47 99 33 128 5			62	04	98	12	115	47	142	•
42 64 2C 90 22 117 21 31 65 10 91 11 118 23 43 65 3 92 23 119 27 43 69 6 94 6 120 77 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 73 25 98 32 128 5			63	36	68	10	116	22	143	•
31 65 10 91 11 118 23 29 25 23 119 27 29 67 3 92 23 119 27 43 67 6 94 6 120 77 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 73 25 98 32 127 22 12 74 47 99 33 128 5			64	22	06	2.2	117	21	144	30
43 66 3 92 23 119 27 29 67 3 93 6 120 77 43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 73 25 98 32 127 22 12 74 47 99 33 128 5			65	10	16		118	23	145	27
29 67 3 93 6 120 77 43 69 6 94 6 121 24 43 70 3 95 14 122 18 23 71 4 96 18 123 9 14 72 24 97 24 126 6 15 73 29 98 32 128 9			99	m	36	23	611	27	146	33
43 69 6 121 24 43 70 3 95 14 122 18 23 71 4 96 18 123 9 14 72 24 97 24 126 6 15 73 25 98 32 127 22 12 74 47 99 33 128 5			67	ודו	63	9	120	77	147	9
43 70 3 95 14 122 18 23 71 4 96 16 123 9 14 72 24 97 24 126 6 15 73 25 98 32 127 22 12 74 47 99 33 128 5			69	¥	96	9	121	24	149	5
23 71 4 96 18 123 9 14 72 24 97 24 126 6 15 73 25 98 32 127 22 12 74 47 99 33 128 5			20	יח	95	4-1	122	18	131	E
14 72 24 97 24 126 15 73 29 98 32 127 12 74 47 99 33 128			7.1	•	96	1.8	123	5	152	E
15 73 25 98 32 127 12 74 47 99 33 128			72	24	76	24	126	w		
12 74 47 99 33 128			73	52	86	(1)	127	22		
	-		7.4	47	66	33	128	5		

STAGE I WING 6 TP-HIGH BURNING RATE AT 1000 FSI

This sample size summary is applicable to figure 72.

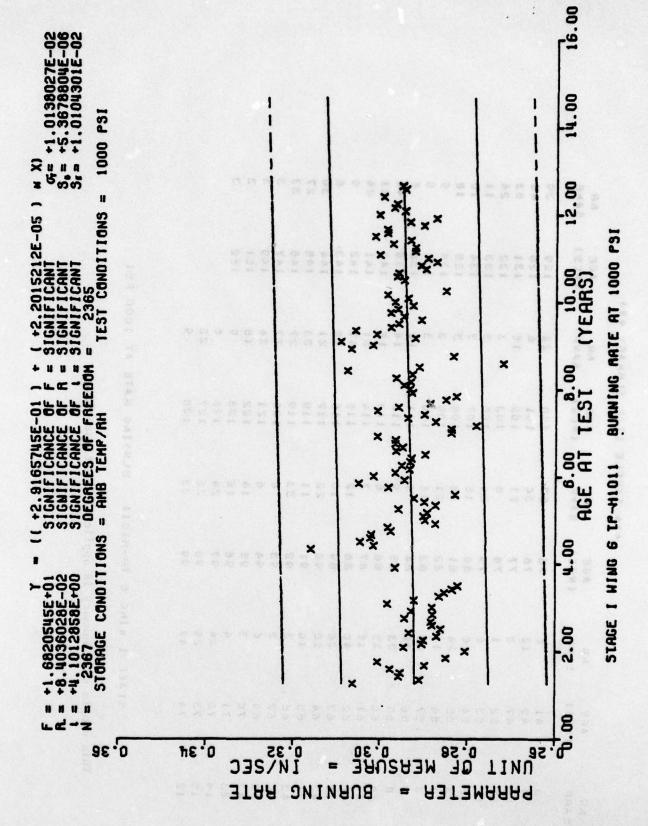


Figure 72

DISTRIBUTION

		me Surveillande	
OOALC			COPIES
MMWRME			2015
MMWRMT			1
DDC (TISIR) Cameron	Station, Alexandria, VA	22314	A 1200
AFPRO, Thiokol Chem:	ical Corporation		2
Wasatch Division			MARKET TRIBUTE
P.O. Box 524			
Brigham City, Ut			
(Cy to R. E. Kes	ating)		
AFRPL (MKPB) Edwards	AFR CA 02522		Astween R
SAC (LGMB) Offutt Al			1
U. S. Naval Ordance	Station, Indian Head, MD	20640	1
Attn: Dr. James			
Fleet Support De	ept., Propulsion		
System Developme	ent Division, Code FS7		
CPIA, Applied Physic	s Laboratory		1
John Hopkins Uni	lvarei tv		
Johns Hopkins Ro			
Laurel, MD 2081			
Attn: Dr. P.L.	Nichole		
Naval Plant Branch F			1
Attn: Mr. David			
P.O. Box 157			
Bacchus Works			
Magna, Utah 840)44		

SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

REPORT DOCUMENTATION	PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER 416(79)	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
Propellant Surveillance Report LGM-30 F & G Stage 1, Phase E Series VII, TP-H1011		S. TYPE OF REPORT & PERIOD COVERED Test Results-Semi-annual 6. PERFORMING ORG. REPORT NUMBER
John A. Thompson	Station, Alement	8. CONTRACT OR GRANT NUMBER(s)
PERFORMING ORGANIZATION NAME AND ADDRESS	arinosagaur 1452 a	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
Propellant Lab Section Directorate of Maintenance OO/ALC Hill AFB, Utah 84056	tats . \$4302	MMEMP Project M82934C-WNL 17514
Directorate of Maintenance OO/ALC Hill AFB, Utah 84056	Can 84302 001-03	
Directorate of Maintenance 00/ALC Hill AFB, Utah 84056 11. CONTROLLING OFFICE NAME AND ADDRESS Service Engineering Division Directorate of Materiel Managemen	CB9 \$4302 ************************************	17514
Directorate of Maintenance 00/ALC Hill AFB, Utah 84056 11. CONTROLLING OFFICE NAME AND ADDRESS Service Engineering Division	t tram Controlling Office)	17514 12. REPORT DATE April 1979 13. NUMBER OF PAGES

16. DISTRIBUTION STATEMENT (of this Report)

Approved for Public Release, Distribution Unlimited

17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)

18. SUPPLEMENTARY NOTES

19. KEY WORDS (Continue on reverse side if necessary and identity by block number)

Solid Propellant Minuteman

This report contains propellant test results from cartons of TP-H1011 bulk propellant representing LGM-30 F and G First Stage Minuteman Motors. This report uses a statistical approach to analyze the bulk carton propellant data. Testing was accomplished in accordance with MMWRM Project M82934CWNL17514.

The data from this test period are combined with data from previous testing and entered into the GO85 computer for storage, analysis and regression analysis. From the statistical analysis of all data tested to date (thirteen

DD 1 JAN 73 1473 EDITION OF 1 NOV 65 IS OBSOLETE

years for F and G), significant degradation of the propellant does not appear likely for at least two years past the oldest data point.

Each point on the regression plot represents the mean of all samples at that particular age. The number of samples at each point is indicated on the sample size summary sheet on the page accompanying each regression plot or group of regression plots. The data range at any age can be found by suitable inquiry of the GO85 system.